



US009101937B2

(12) **United States Patent**
Kitamura et al.

(10) **Patent No.:** **US 9,101,937 B2**
(45) **Date of Patent:** **Aug. 11, 2015**

(54) **PRECISE TEMPERATURE CONTROLLING UNIT AND METHOD THEREOF**

USPC 219/494, 497, 505, 521, 388, 385;
422/65, 67; 435/287 J, 290, 285.1,
435/286.1, 288.1

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See application file for complete search history.

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(56) **References Cited**

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 458 days.

U.S. PATENT DOCUMENTS

4,865,986 A * 9/1989 Coy et al. 435/285.1
5,161,609 A * 11/1992 Dutertre et al. 165/267
5,446,263 A * 8/1995 Eigen et al. 219/521
6,015,534 A * 1/2000 Atwood 422/550

(Continued)

(21) Appl. No.: **13/504,732**

(22) PCT Filed: **Oct. 29, 2010**

FOREIGN PATENT DOCUMENTS

(86) PCT No.: **PCT/JP2010/069290**

DE 19646114 B4 9/2004
JP 04-501530 A 3/1992

§ 371 (c)(1),

(2), (4) Date: **May 22, 2012**

(Continued)

OTHER PUBLICATIONS

(87) PCT Pub. No.: **WO2011/052723**

PCT Pub. Date: **May 5, 2011**

International Search Report issued in corresponding PCT International Application No. PCT/JP2010/069290, mailed Jan. 18, 2011.
Extended European Search Report issued in corresponding European Patent Application No. 10826853.3 dated Jul. 16, 2014.

Primary Examiner — Mark Paschall

(65) **Prior Publication Data**

US 2012/0247725 A1 Oct. 4, 2012

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(30) **Foreign Application Priority Data**

Oct. 30, 2009 (JP) 2009-251040

(57)

ABSTRACT

(51) **Int. Cl.**

H05B 1/02 (2006.01)

B01L 7/00 (2006.01)

B01L 3/00 (2006.01)

A temperature controlling unit (X1) includes a holder (11) for a liquid receiver (40), a heating block (12) for heating the liquid in the liquid receiver (40), and a cooling block (13) for cooling the liquid in the liquid receiver (40). The holder (11) maintains a first temperature for keeping the temperature of the liquid in the liquid receiver (40) at a lower target temperature. The heating block (12) maintains a second temperature higher than a higher target temperature above the lower target temperature. The cooling block (13) maintains a third temperature lower than the lower target temperature. A temperature controlling method of the present invention includes a heating step for bringing a heating block (12) into contact with the liquid receiver (40) held by the holder (11) and a cooling step for bringing a cooling block (13) into contact with the liquid receiver (40) held by the holder (11).

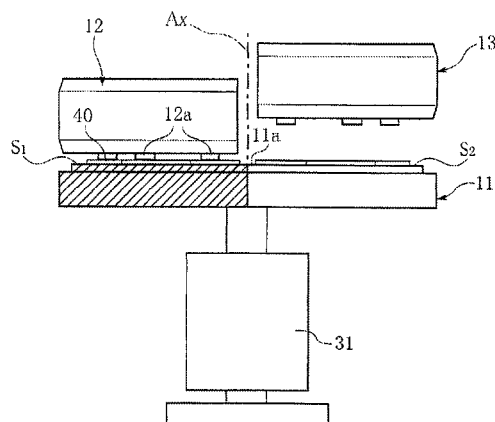
13 Claims, 16 Drawing Sheets

(52) **U.S. Cl.**

CPC **B01L 7/525** (2013.01); **B01L 3/5027** (2013.01); **B01L 2300/0816** (2013.01); **B01L 2300/1805** (2013.01); **B01L 2300/185** (2013.01)

(58) **Field of Classification Search**

CPC H05B 1/025; H05B 1/0244; B01L 2300/0816; B01L 2300/1805; B01L 2300/185



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(56)

References Cited

FOREIGN PATENT DOCUMENTS

U.S. PATENT DOCUMENTS

7,030,340	B2	4/2006	Knoche	
7,182,130	B2 *	2/2007	Ohki	165/263
7,745,205	B2 *	6/2010	Wittwer et al.	435/287.2
7,754,473	B2 *	7/2010	Nurmi et al.	435/287.1
2008/0286161	A1 *	11/2008	Heaney et al.	422/102
2009/0001973	A1	1/2009	May et al.	
2013/0323796	A1 *	12/2013	Chesnut et al.	435/91.5

JP	06-277036	A	10/1994
JP	08-117590	A	5/1996
JP	2000-270837	A	10/2000
JP	2002-306154	A	10/2002
JP	2006-238848	A	9/2006
WO	2008/027398	A2	3/2008
WO	2009/000604	A1	12/2008

* cited by examiner

FIG. 1

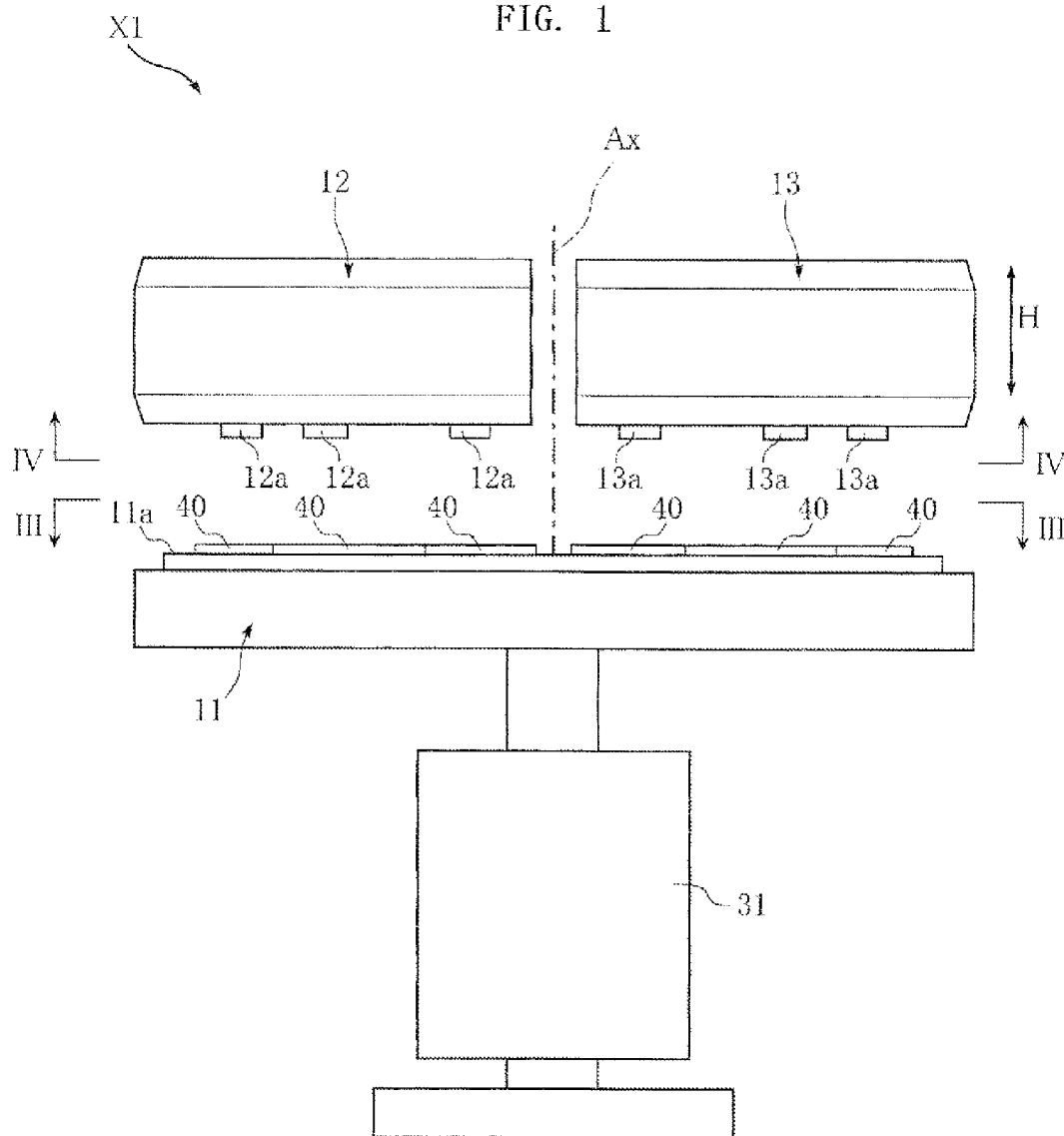


FIG. 2

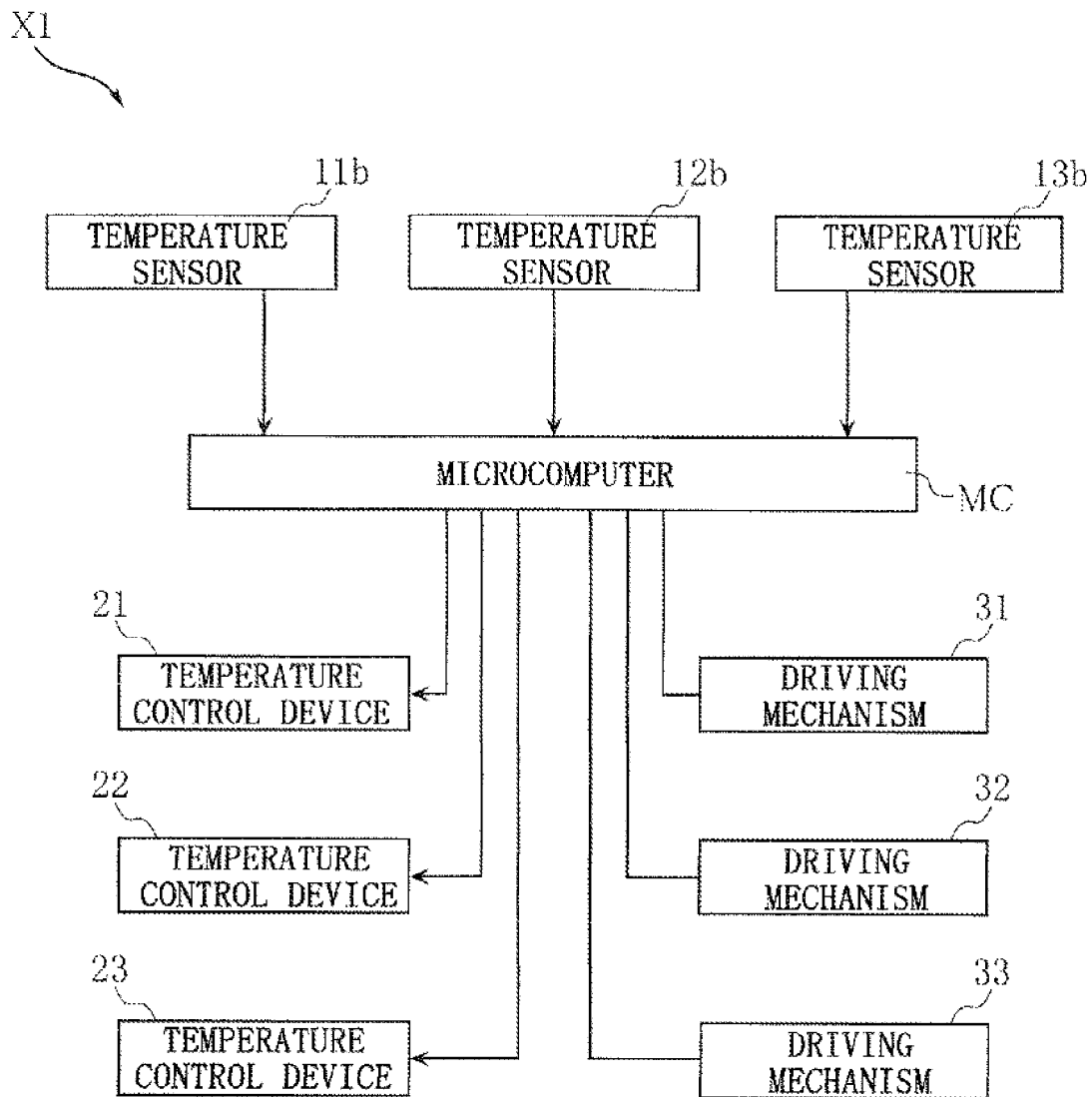


FIG. 3

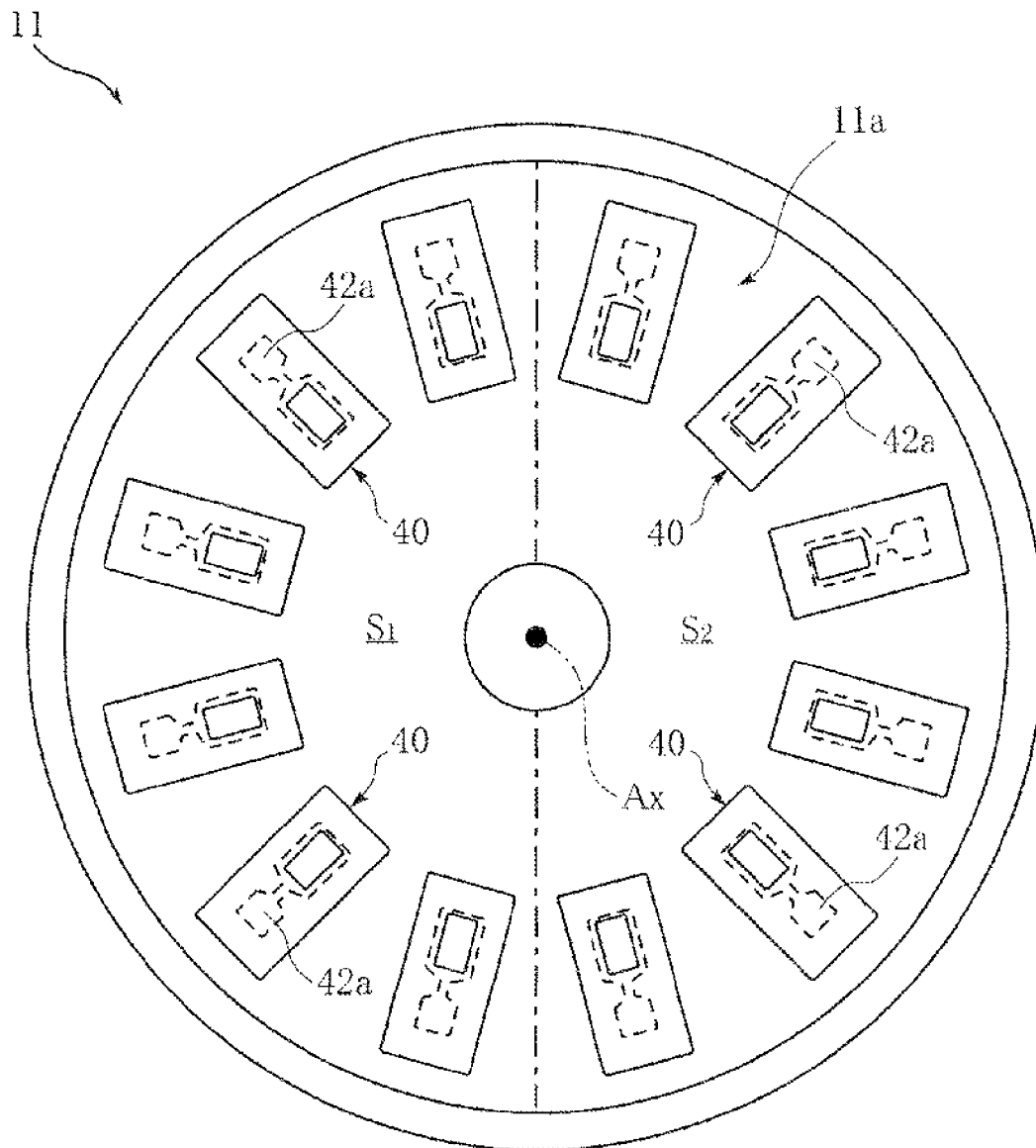
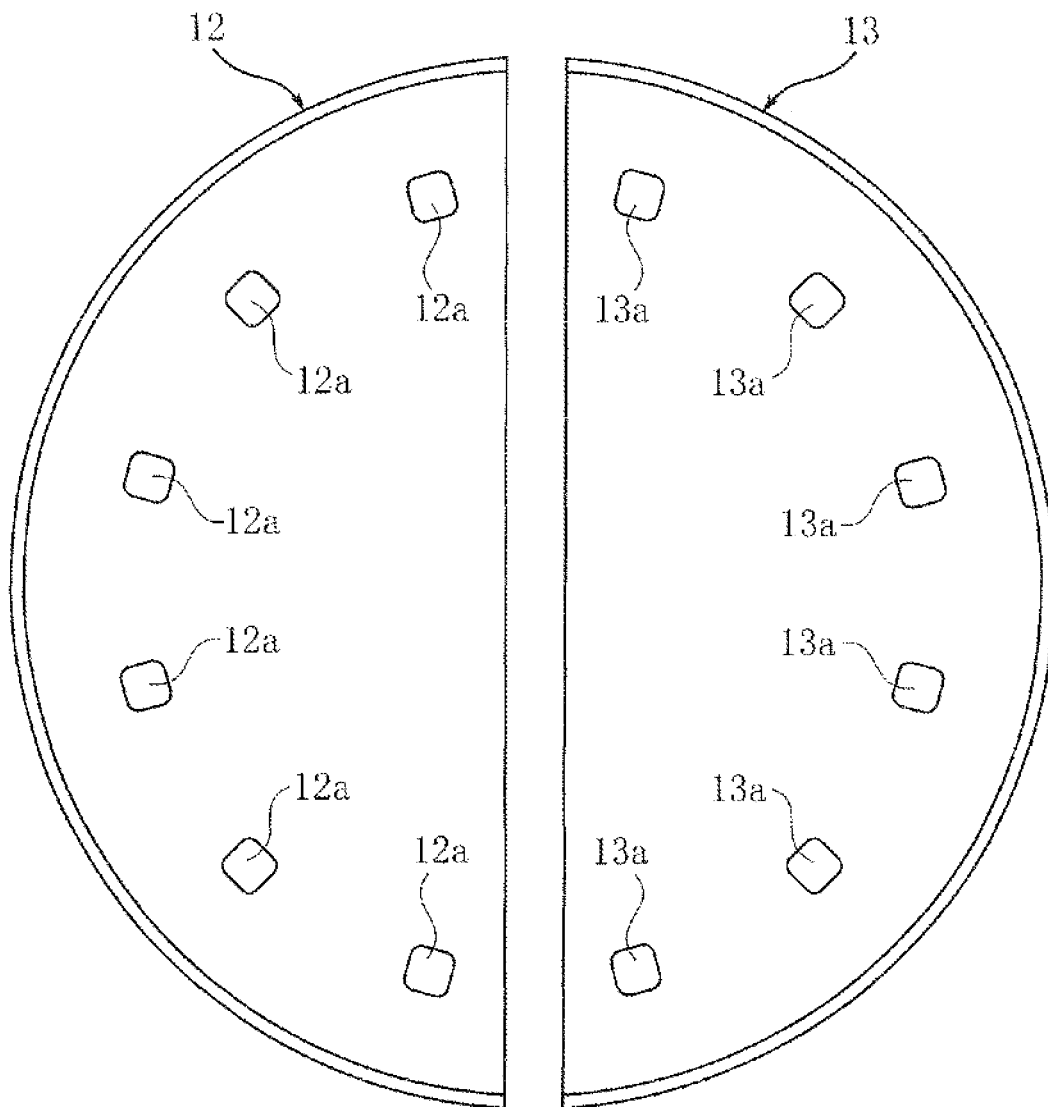


FIG. 4



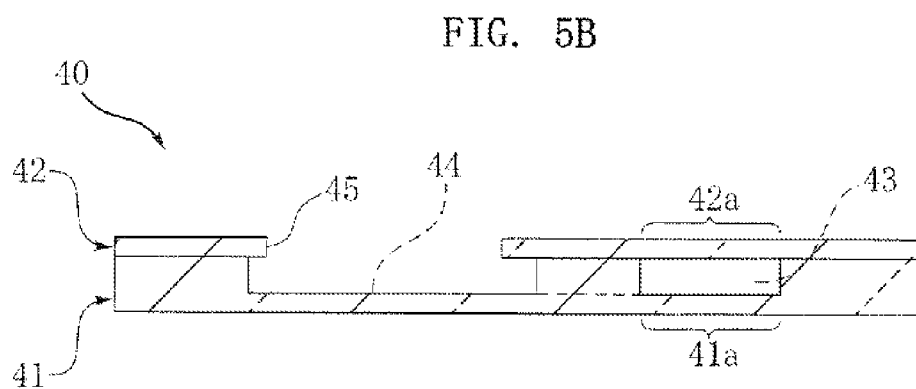
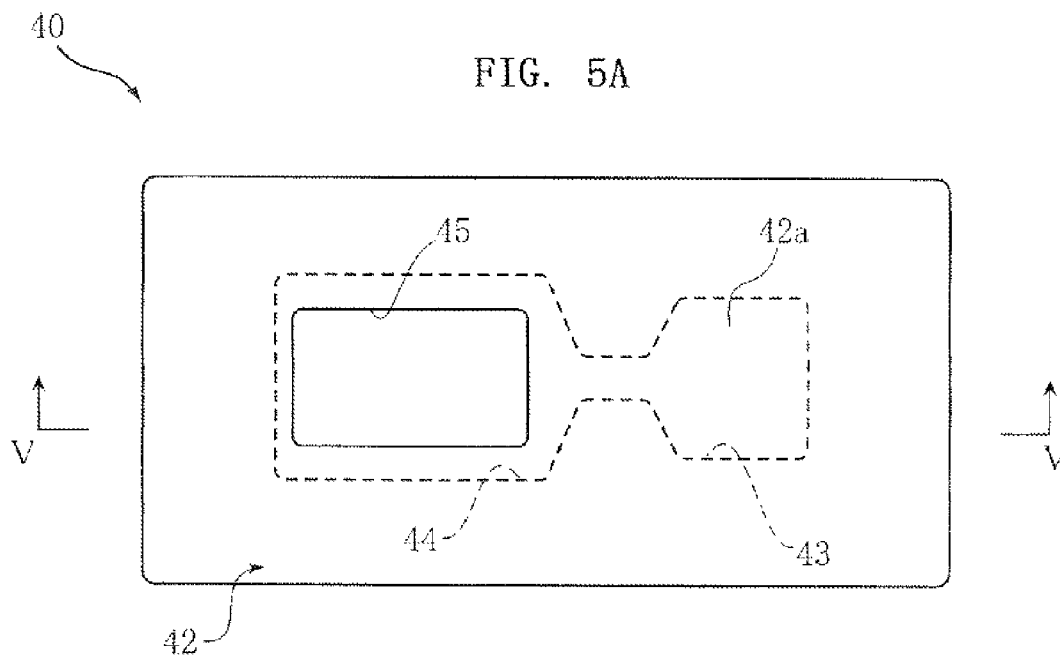


FIG. 6A

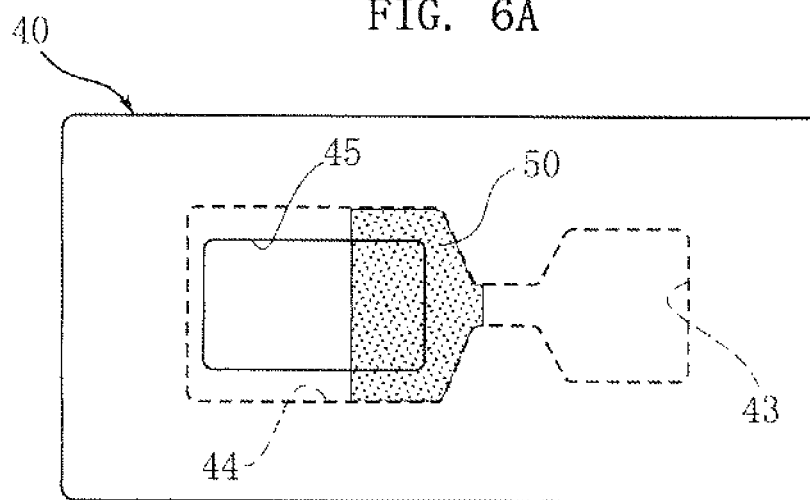


FIG. 6B

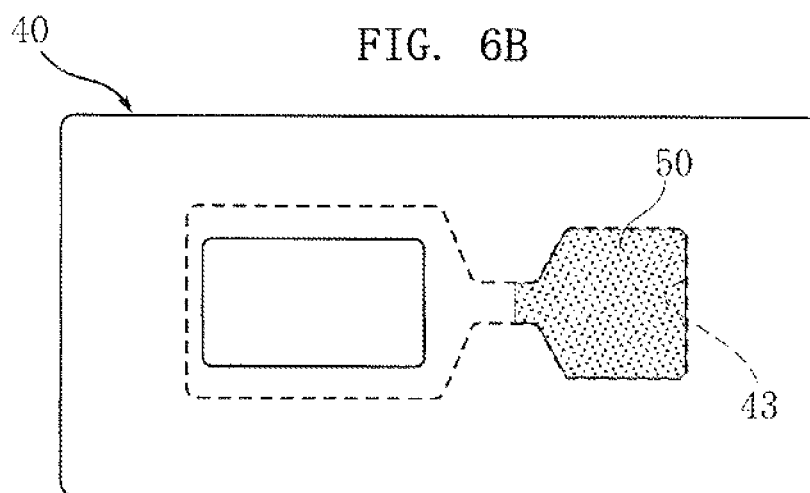


FIG. 6C

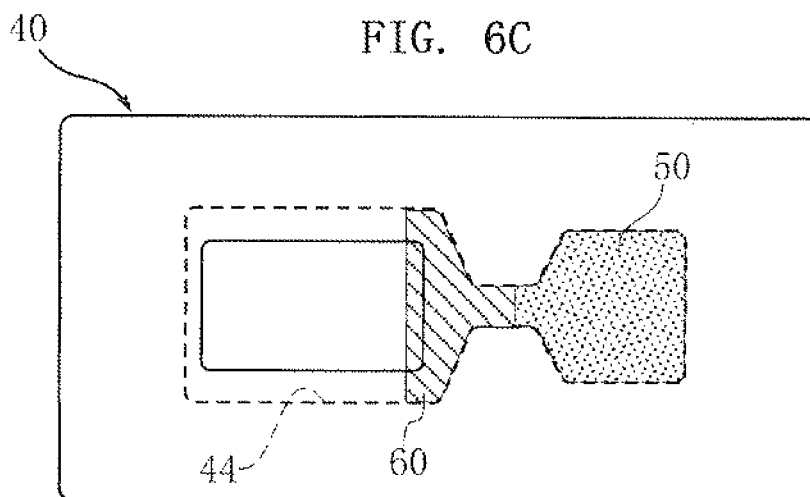


FIG. 7

	STEP 1	STEP 2	STEP 3	STEP 4	STEP 5	STEP 6
1st GROUP	TEMPERATURE INCREASE STEP	TEMPERATURE REDUCTION STEP	TEMPERATURE MAINTAINING STEP	TEMPERATURE MAINTAINING STEP	TEMPERATURE MAINTAINING STEP	TEMPERATURE INCREASE STEP
2nd GROUP	STANDBY	TEMPERATURE INCREASE STEP		TEMPERATURE REDUCTION STEP	TEMPERATURE MAINTAINING STEP	

FIG. 8

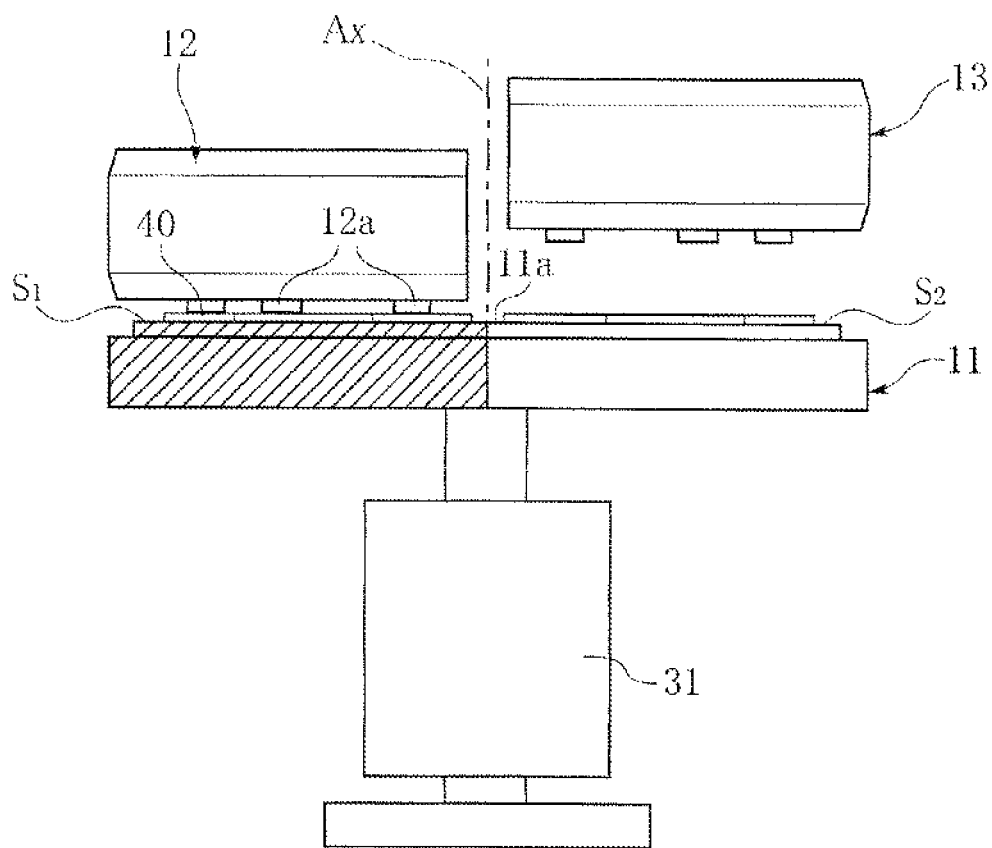


FIG. 9

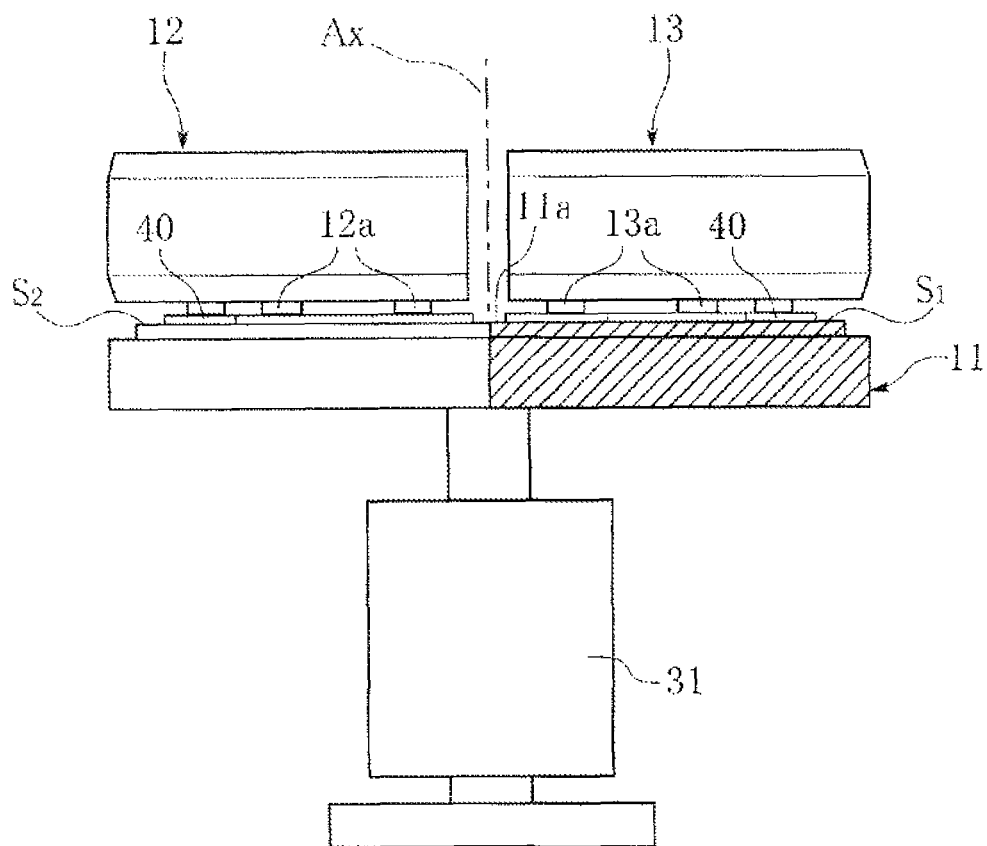


FIG. 10

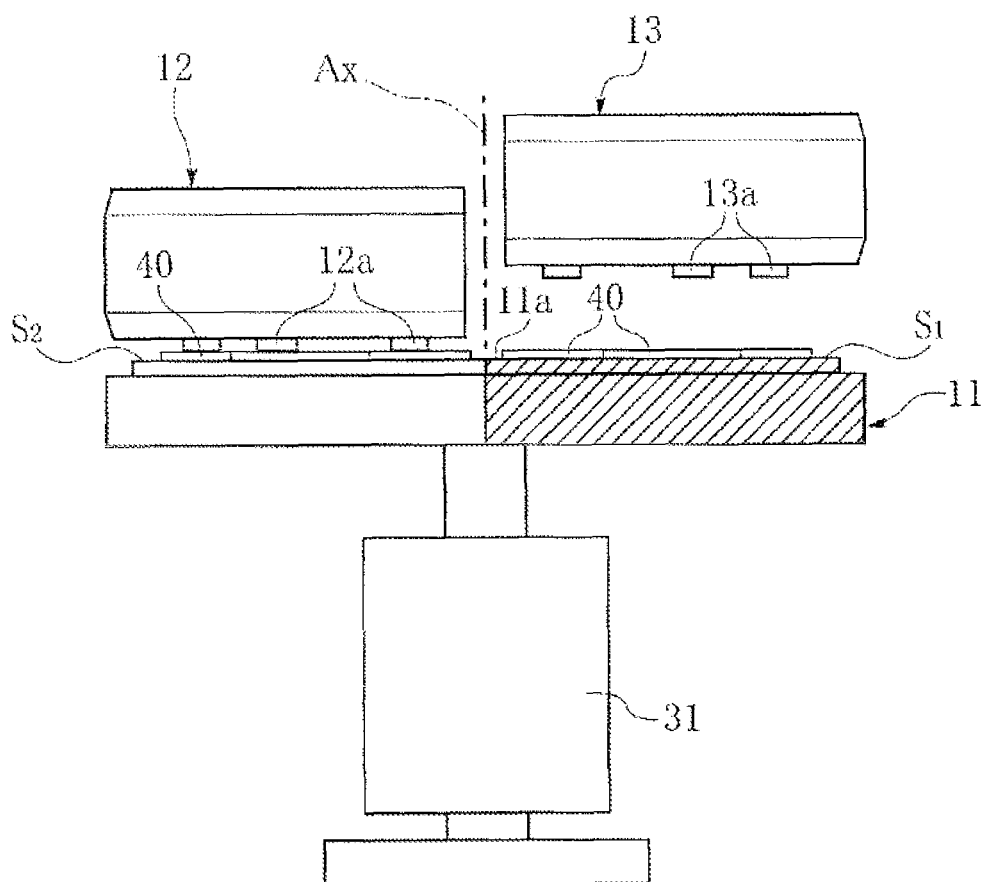


FIG. 11

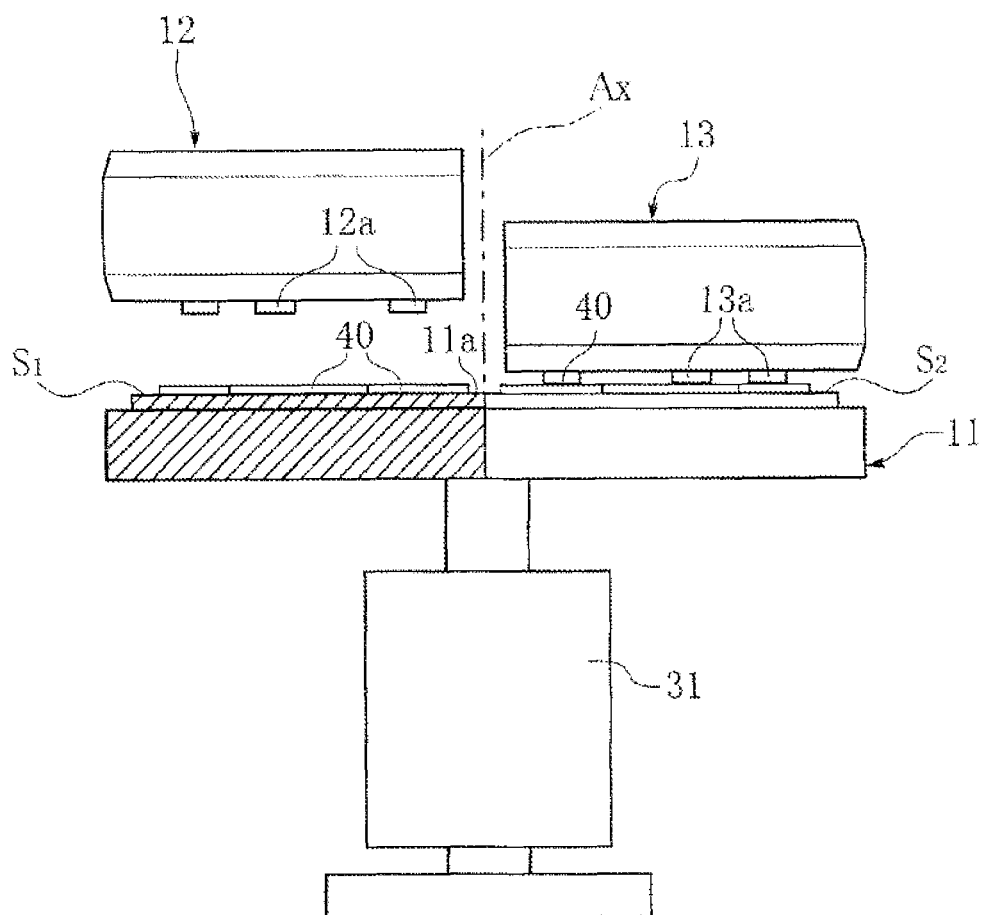


FIG. 12

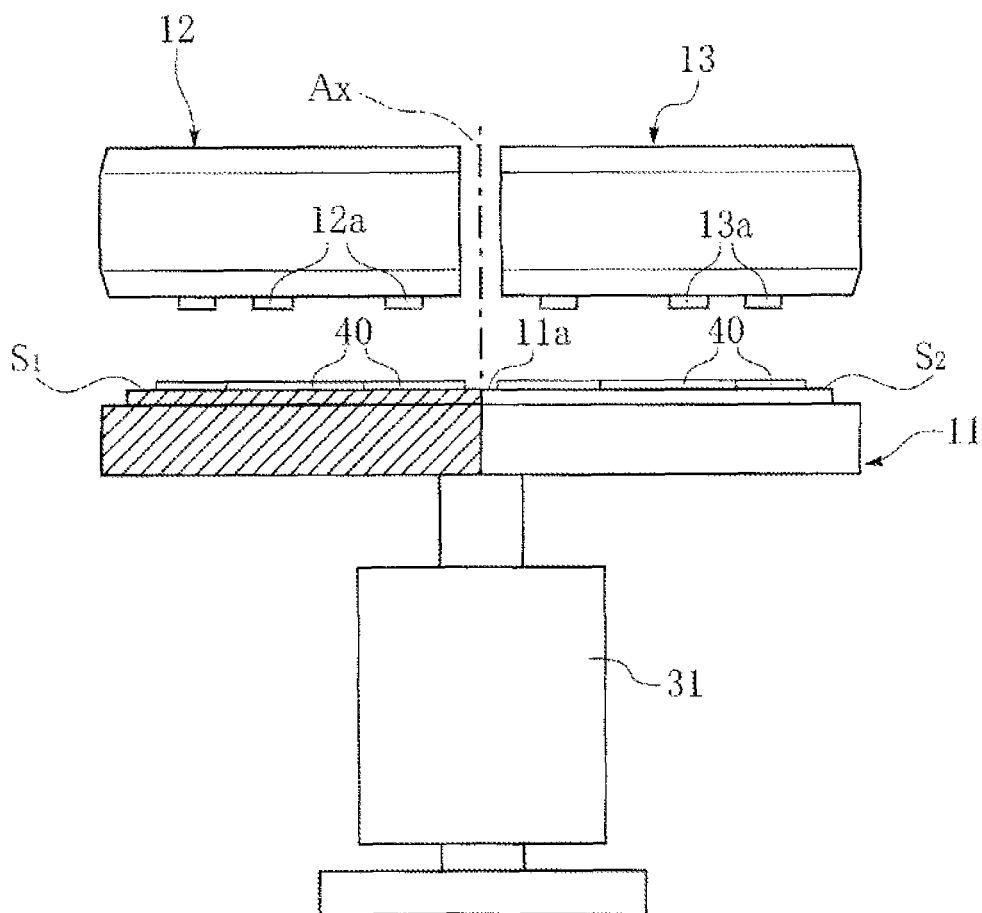


FIG. 13

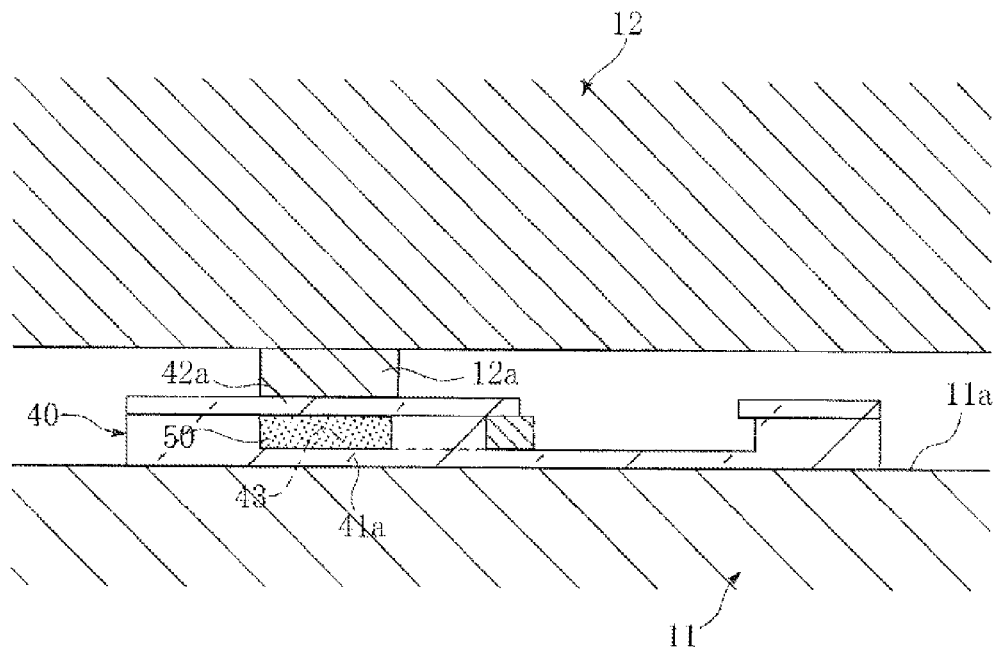


FIG. 14

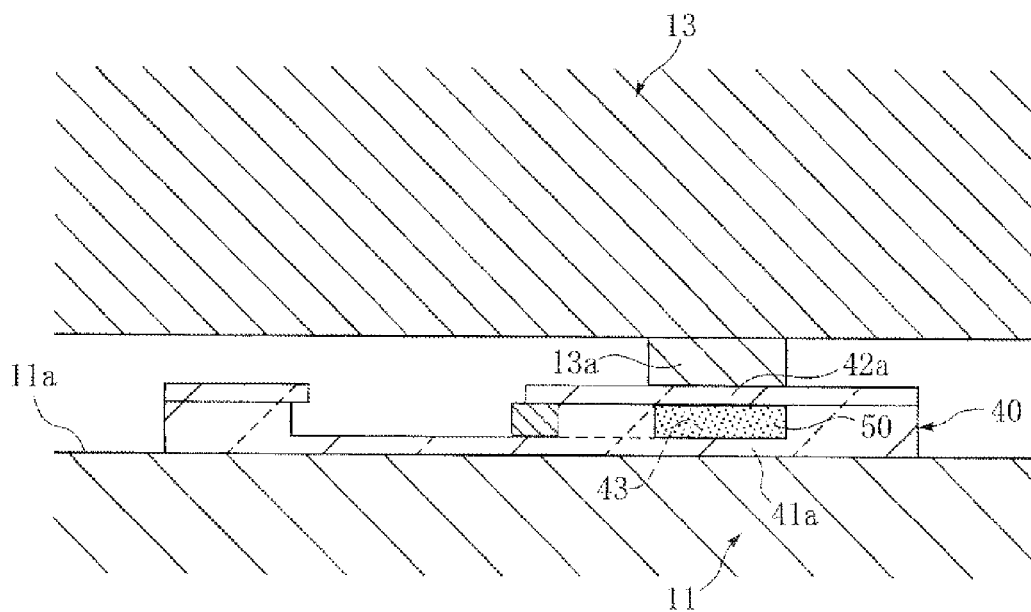


FIG. 15

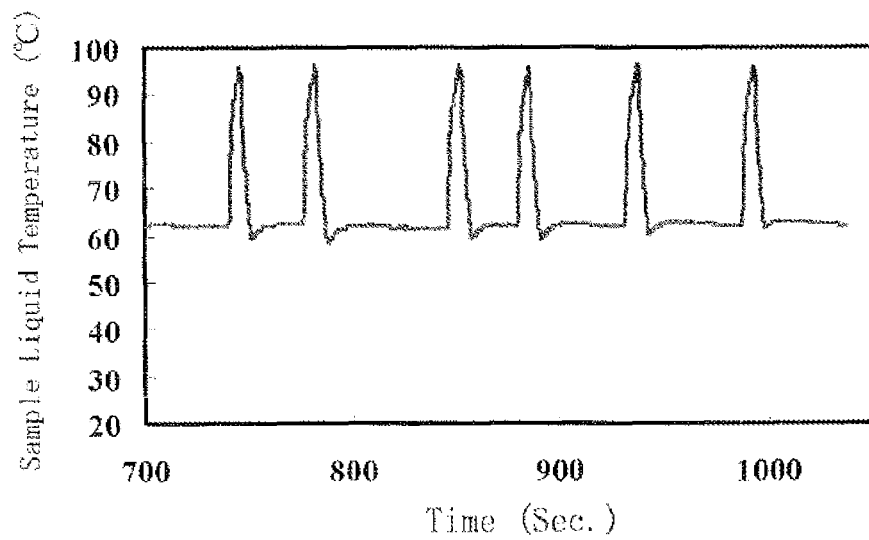


FIG. 16

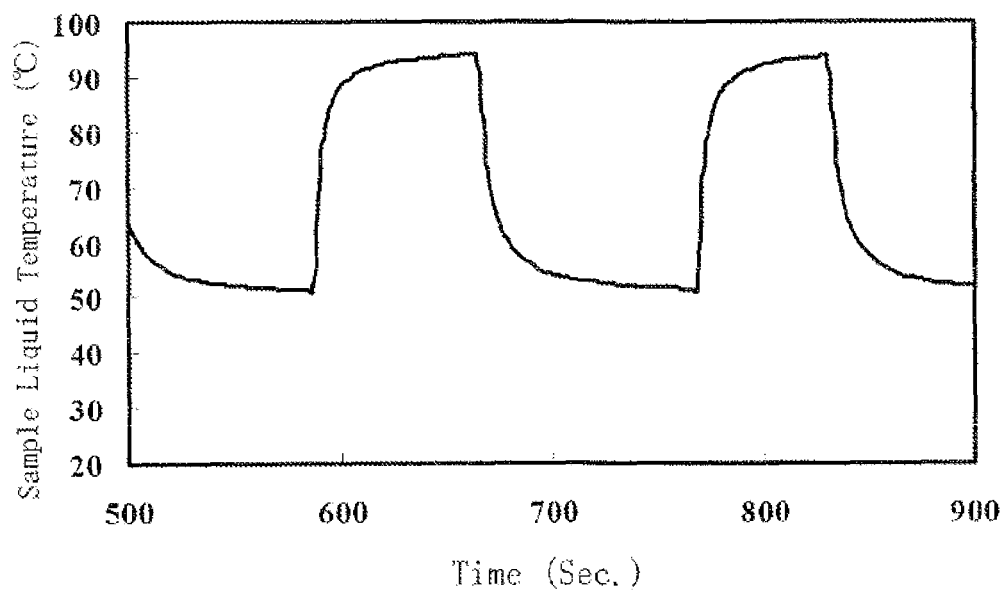


FIG. 17

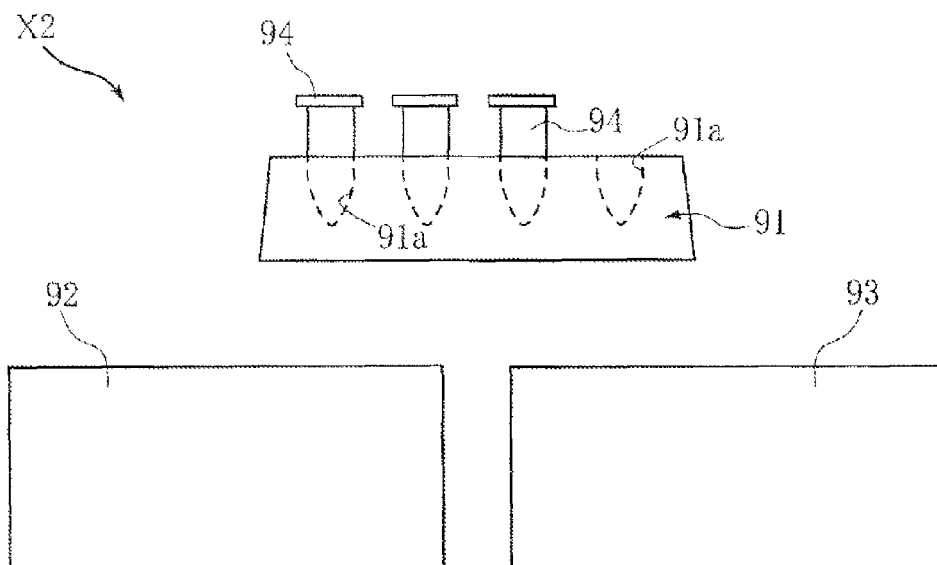
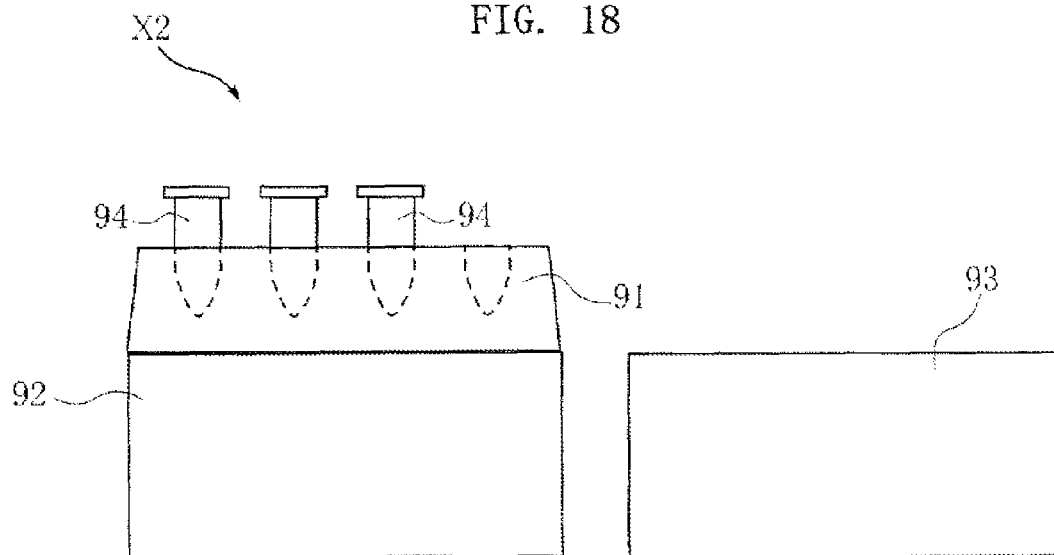


FIG. 18



X2
↘

FIG. 19

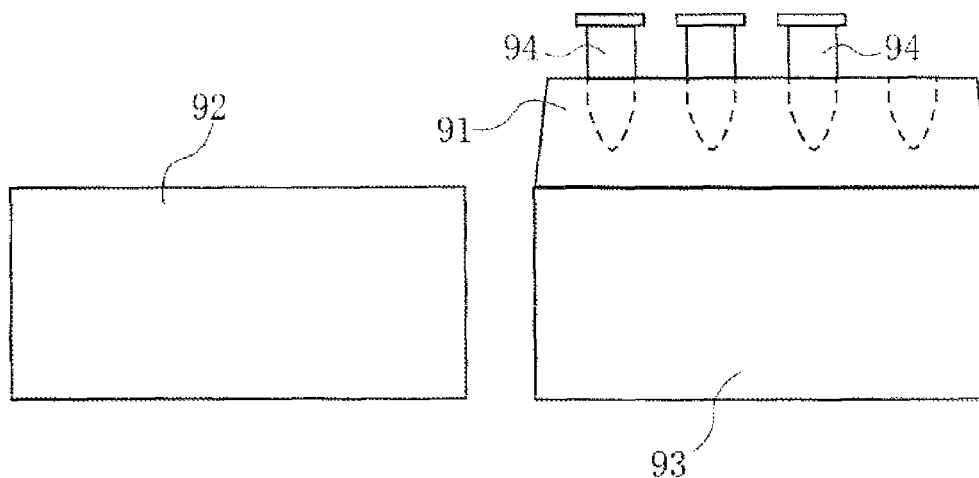
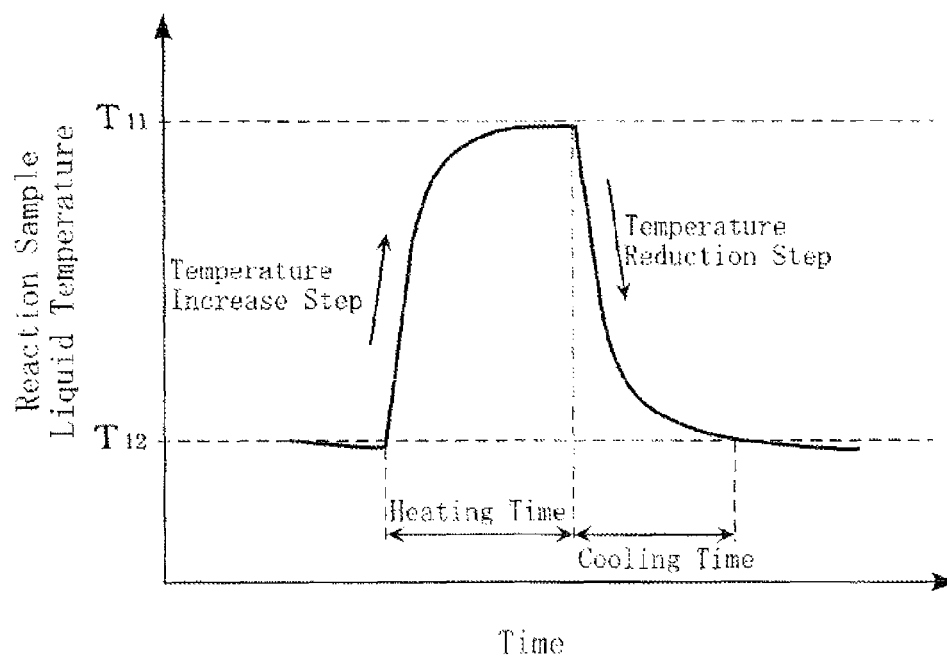


FIG. 20



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PRECISE TEMPERATURE CONTROLLING UNIT AND METHOD THEREOF

The present application is a U.S. National Phase Application of International Application No. PCT/JP2010/069290, filed Oct. 29, 2010, which claims the benefit of priority of Japanese Application No. 2009-251040 filed Oct. 30, 2009, the disclosures of which are incorporated herein by reference in their entireties.

TECHNICAL FIELD

The present invention relates to a temperature controlling unit that can be used as a PCR machine, for example. The present invention also relates to a temperature controlling method that can be used for PCR methods.

BACKGROUND ART

Apparatuses for controlling the temperature of a liquid are currently used in various technical fields. For instance, in biochemistry, temperature controlling units for controlling the temperature of a sample liquid are used. Examples of known temperature controlling units include a PCR machine for performing a PCR (polymerase chain reaction) method. As to PCR methods, description is given in e.g. Patent Documents 1 and 2 identified below.

FIG. 17 shows an example of conventional PCR machine. The illustrated PCR machine X2 includes a holding block 91, a heating block 92 and a cooling block 93. In the PCR machine X2, a cycle including thermal denaturation, annealing and elongation is repeated a plurality of times.

The holding block 91 is formed with a plurality of recesses 91a for receiving tubes 94. Each of the tubes 94 contains a reaction sample liquid or the like for performing a PCR method. The reaction sample liquid contains template DNA, primer DNA, DNA polymerase, and dNTP. The holding block 91 is transferred by a transfer member (not shown) to a position above the heating block 92 (FIG. 18) or a position above the cooling block 93 (FIG. 19). The heating block 92 is provided for supplying heat to the holding block 91 and thermally connected to a heating device (not shown). The cooling block 93 is provided for taking heat from the holding block 91 and thermally connected to a heat-absorbing device (not shown).

In the PCR machine X2, a PCR method is performed as described below, for example.

First, the holding block 91 is placed on the heating block 92 and heated by the heating block 92 (temperature increase step). In this step, the heating block 92 is kept at a thermal denaturation temperature T_{11} (e.g. 95° C.) by the heating device.

When the holding block 91 substantially reaches the thermal denaturation temperature T_{11} , the reaction sample liquid in the tubes 94 held by the holding block 91 also reaches the denaturation temperature T_{11} , so that a thermal denaturation step starts. In the thermal denaturation step, two strands of a template DNA are separated from each other.

After the thermal denaturation step, the holding block 91 is transferred to and placed on the cooling block 93 and cooled by the cooling block 93 (temperature reduction step). In this step, the cooling block 93 is kept at an annealing/elongation temperature T_{12} (e.g. 60° C.) by the operation of the heat-absorbing device, not shown.

When the holding block 91 substantially reaches the annealing/elongation temperature T_{12} , the reaction sample liquid in the tubes 94 held by the holding block 91 also

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reaches the annealing/elongation temperature T_{12} , so that an annealing/elongation step (the step in which annealing and elongation proceed at the same time) starts. In the annealing step, each single-stranded DNA of the template combines with a primer (containing a base sequence complementary to part of the single-stranded DNA). In the elongation step, at the 3' end of the primer combined with the single-stranded DNA of the template, a DNA strand containing a base sequence complementary to a single-stranded DNA is elongated or synthesized.

In the PCR machine X2, the cycle including the above-described steps is repeated a plurality of times, whereby a piece of DNA having a predetermined base sequence is amplified.

Patent Document 1: JP-A-4-501530

Patent Document 2: JP-A-6-277036

FIG. 20 is a graph showing an example of temperature change of a reaction sample liquid in each cycle of the above-described PCR method performed by the PCR machine X2. As shown in the graph of FIG. 20, in the temperature increase step, the temperature increase speed in a temperature range close to the target temperature (thermal denaturation temperature T_{11}) is considerably low as compared with the temperature increase speed in the initial stage of the temperature increase step. In this way, with the PCR machine X2, the reaction sample liquid reaches the thermal denaturation temperature T_{11} after going through the temperature range in which the temperature increase speed is considerably low. Thus, it is necessary to secure sufficient time for the temperature increase step. Moreover, in the temperature reduction step, the temperature reduction speed in a temperature range close to the target temperature (the annealing/elongation temperature T_{12}) is considerably low as compared with the temperature reduction speed in the initial stage of the temperature reduction step. In this way, with the PCR machine X2, the reaction sample liquid reaches the annealing/elongation temperature T_{12} after going through the temperature range in which the temperature reduction speed is considerably low. Thus, it is necessary to secure sufficient time for the temperature reduction step as well. Thus, the PCR machine X2 is not suitable for completing the temperature increase step and the temperature reduction step in a short period of time. In other words, the PCR machine X2 is not suitable for quickly changing the temperature of a reaction sample liquid (liquid).

SUMMARY OF THE INVENTION

The present invention has been proposed under the circumstances described above. It is therefore an object of the present invention to provide a temperature controlling unit and a temperature controlling method suitable for quickly changing the temperature of a liquid.

According to a first aspect of the present invention, there is provided a temperature controlling unit. The temperature controlling unit comprises a holder, a heating block and a cooling block. The holder is provided for holding a liquid receiver containing a liquid in contact with the liquid receiver and is configured to maintain a first temperature (T_1) for keeping the temperature of the liquid at a lower target temperature (T_L). The heating block is provided for increasing the temperature of the liquid through contact with the liquid receiver. The heating block is movable relative to the liquid receiver and configured to maintain a second temperature (T_2) higher than a higher target temperature (T_H) that is higher than the lower target temperature (T_L). The cooling block is provided for reducing the temperature of the liquid through contact with the liquid receiver. The cooling block is

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movable relative to the liquid receiver and configured to maintain a third temperature (T_3) lower than the lower target temperature (T_L).

The liquid or target, subjected to temperature control by the temperature controlling unit, is received in a liquid receiver, and the liquid receiver is held by a holder. During the operation of the unit, the temperature of the holder is set to and maintained at a first temperature for keeping the temperature of the liquid in the liquid receiver at a lower target temperature. Here, the first temperature for keeping the temperature of the liquid in the liquid receiver at a lower target temperature, is a temperature by which the temperature of the liquid in the liquid receiver will be changed and subsequently kept at the lower target temperature when a sufficient time has elapsed in a state where no heat transfer occurs from the heating block to the liquid receiver or the liquid and no heat transfer from the liquid receiver or the liquid to the cooling block. The above-defined first temperature may be set depending on, for example, the lower target temperature, environmental temperature, thermal conductivity of the material for the liquid receiver, and the structure and heat dissipation ability of the liquid receiver. For instance, when the lower target temperature is equal or substantially equal to the environmental temperature, it may be suitable to set the first temperature of the holder to be equal to the lower target temperature. When the lower target temperature is considerably higher than the environmental temperature, it may be suitable to set the first temperature of the holder to be higher than the lower target temperature. When the lower target temperature is considerably lower than the environmental temperature, it may be suitable to set the first temperature of the holder to be lower than the lower target temperature.

The temperature increase by the temperature controlling unit is performed by causing the heating block, which is movable relative to the liquid receiver, to come closer to and into contact with the liquid receiver. At least during the temperature increase step, the temperature of the heating block is set to and maintained at a second temperature. It is preferable that the temperature of the heating block is maintained at the second temperature during the operation of the unit. The second temperature is higher than a higher target temperature (that is higher than the lower target temperature) for the liquid in the liquid receiver. For instance, in the temperature increase step by the temperature control unit, heat transfer from the heating block to the liquid receiver or the liquid is stopped by separating the heating block from the liquid receiver when the temperature of the liquid in the liquid receiver has reached the higher target temperature.

The temperature reduction by the temperature controlling unit is performed by causing the cooling block, which is movable relative to the liquid receiver held by the holder kept at the first temperature, to come closer to and into contact with the liquid receiver. At least during the temperature reduction step, the temperature of the cooling block is set to and maintained at a third temperature. It is preferable that the temperature of the cooling block is maintained at the third temperature during the operation of the unit. The third temperature is lower than the lower target temperature for the liquid in the liquid receiver. When the first temperature of the holder is lower than the lower target temperature, the third temperature of the cooling block is set to be lower than the first temperature. For instance, in the temperature reduction step by the temperature control unit, heat transfer from the liquid receiver or the liquid to the cooling block is stopped by separating the cooling block from the liquid receiver before the temperature of the liquid in the liquid receiver reaches the lower target temperature.

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Preferably, in the first aspect of the present invention, the first temperature of the holder may be equal to the lower target temperature; or higher than the lower target temperature and lower than the higher target temperature; or lower than the lower target temperature and higher than the third temperature. The first temperature of the holder may be set depending on the lower target temperature, environmental temperature, thermal conductivity of the material for the liquid receiver, and the structure and heat dissipation ability of the receiver, such that the temperature of the liquid in the liquid receiver is ultimately kept at the lower target temperature when a sufficient time has elapsed in a state where no heat transfer occurs from the heating block to the liquid receiver or the liquid and no heat transfer from the liquid receiver or the liquid to the cooling block.

Preferably, the heating block is configured to come into contact with a side of the liquid receiver that is opposite from the holder, and the cooling block is configured to come into contact with a side of the liquid receiver that is opposite from the holder.

Preferably, the holder includes a holding surface for holding the liquid receiver and is rotatable about an axis perpendicular to the holding surface. In this case, each of the heating block and the cooling block faces the holding surface of the holder and is movable toward and away from the holding surface.

Preferably, the holding surface includes a first region for holding a liquid receiver containing a liquid in contact with the liquid receiver and a second region for holding a liquid receiver containing a liquid in contact with the liquid receiver. In this case, each of the heating block and the cooling block is configured to move closer to and come into contact with the liquid receiver held in the first region when facing the first region and configured to move closer to and come into contact with the liquid receiver held in the second region when facing the second region.

Preferably, the holding surface includes a first region for holding a plurality of liquid receivers each containing a liquid in contact with the liquid receivers and a second region for holding a plurality of liquid receivers each containing a liquid in contact with the liquid receivers. In this case, each of the heating block and the cooling block is configured to move closer to and come into contact with the plurality of liquid receivers held in the first region when facing the first region and configured to move closer to and come into contact with the plurality of liquid receivers held in the second region when facing the second region.

Preferably, the first region and the second region are configured to hold the plurality of liquid receivers such that the liquid receivers are arranged on a circle (imaginary circle) around the axis.

Preferably, the liquid receiver includes a first cell wall and a second cell wall facing and spaced from each other, and a cell for receiving a liquid defined between the first cell wall and the second cell wall. In this case, the holder is configured to hold the liquid receiver in contact with the first cell wall of the liquid receiver. The heating block is configured to come into contact with the second cell wall of the liquid receiver, and the cooling block is also configured to come into contact with the second cell wall of the liquid receiver.

Preferably, the maximum dimension of the cell in a direction perpendicular to the spacing direction in which the first cell and the second cell are spaced from each other is larger than the maximum dimension of the cell in the spacing direction. That is, it is preferable that the cell for receiving a liquid as the target for temperature control is shallow.

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Preferably, each of the heating block and the cooling block includes a projection for coming into contact with the second cell wall. The heating block with a projection for coming into contact with the second cell wall is suitable for allowing local heat transfer from the heating block to the liquid in the cell. The cooling block with a projection for coming into contact with the second cell wall is suitable for allowing local heat transfer from the liquid in the cell to the cooling block. Realizing local heat transfer contributes to enhancement of heat transfer efficiency.

According to a second aspect of the present invention, there is provided a temperature controlling method. The temperature controlling method includes a temperature increase step and a temperature reduction step. In the temperature increase step, a heating block kept at a heating temperature (corresponding to the second temperature in the first aspect) higher than a higher target temperature for a liquid is brought into contact with a liquid receiver containing the liquid to increase the temperature of the liquid. In the temperature reduction step, a cooling block kept at a cooling temperature (corresponding to the third temperature in the first aspect) lower than a lower target temperature that is lower than the higher target temperature is brought into contact with the liquid receiver to reduce the temperature of the liquid. The temperature reduction step is performed with a lower target temperature maintaining member held in contact with the liquid receiver. The lower target temperature maintaining member is kept at any one of a temperature equal to the lower target temperature, a temperature higher than the lower target temperature and lower than the higher target temperature, and a temperature lower than the lower target temperature and higher than the cooling temperature. (The temperature of the lower target temperature maintaining member corresponds to the first temperature in the first aspect.)

The temperature controlling method can be carried out properly by the above-described temperature controlling unit according to the first aspect. The temperature controlling method is suitable for quickly changing (increasing or reducing) the temperature of a liquid and also suitable for controlling the temperature of a liquid precisely to a higher target temperature or a lower target temperature. The temperature controlling method is suitable for the application to e.g. a PCR method that requires quick and precise temperature control.

Preferably, in the second aspect of the present invention, the heating block is separated from the liquid receiver in the temperature increase step when the temperature of the liquid has reached the higher target temperature. This is suitable for controlling the temperature of a liquid during the temperature increase precisely to the higher target temperature in the temperature increase step.

Preferably, in the temperature reduction step, the cooling block is separated from the liquid receiver before the temperature of the liquid reaches the lower target temperature. This contributes to controlling the temperature of a liquid during the temperature reduction precisely to the lower target temperature in the temperature reduction step.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 shows part of the structure of a temperature controlling unit according to the present invention;

FIG. 2 shows part of a functional block diagram of the temperature controlling unit according to the present invention;

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FIG. 3 is a view seen in the direction of arrow in FIG. 1, showing a holding surface of a rotation table, with sample liquid chips held thereon;

FIG. 4 is a view seen in the direction of arrow IV-IV in FIG. 1, showing a surface of a heating block on the rotation table side and a surface of the cooling block on the rotation table side;

FIG. 5A is an enlarged plan view of a sample liquid chip;

FIG. 5B is a sectional view taken along lines V-V in FIG. 5A;

FIG. 6A shows a process in introducing sample liquid into a sample liquid chip;

FIG. 6B shows a process in introducing sample liquid into a sample liquid chip;

FIG. 6C shows a process in introducing sample liquid into a sample liquid chip;

FIG. 7 shows part of a table of steps in parallel temperature control performed by the temperature controlling unit according to the present invention;

FIG. 8 shows the state of the temperature controlling unit in Steps 1 and 6;

FIG. 9 shows the state of the temperature controlling unit in Step 2;

FIG. 10 shows the state of the temperature controlling unit in Step 3;

FIG. 11 shows the state of the temperature controlling unit in Step 4;

FIG. 12 shows the state of the temperature controlling unit in Step 5;

FIG. 13 is an enlarged sectional view showing part of the temperature controlling unit during a temperature increase step;

FIG. 14 is an enlarged sectional view showing part of the temperature controlling unit during a temperature reduction step;

FIG. 15 is a graph showing part of temperature change of a sample liquid in an Example;

FIG. 16 is a graph showing part of temperature change of a sample liquid in a Comparative Example;

FIG. 17 shows the structure of a conventional PCR machine;

FIG. 18 shows the PCR machine of FIG. 17 during a temperature increase step;

FIG. 19 shows the PCR machine of FIG. 17 during a temperature reduction step; and

FIG. 20 is a graph showing an example of temperature change of a reaction sample liquid in each cycle of the PCR method performed by the PCR machine of FIG. 17.

BEST MODE FOR CARRYING OUT THE INVENTION

A temperature controlling unit X1 according to the present invention is shown in FIGS. 1-4. FIG. 1 shows part of the structure of the temperature controlling unit X1. FIG. 2 shows part of a functional block diagram of the temperature controlling unit X1. FIGS. 3 and 4 are views seen in the direction of arrows III-III and arrows IV-IV in FIG. 1, respectively.

The temperature controlling unit X1 includes a rotation table 11, a heating block 12, a cooling block 13, temperature controlling devices 21, 22, 23, driving mechanisms 31, 32, 33 and a microcomputer MC. The temperature controlling unit X1 is designed to perform a PCR method that repeats a cycle including thermal denaturation, annealing and elongation a plurality of times.

The rotation table 11 functions as a holder and a lower target temperature maintaining member. The rotation table 11

includes a holding surface **11a** for holding sample liquid chips **40** in contact with the sample liquid chips **40**. The rotation table **11** is rotatable about an axis **Ax** (perpendicular to the holding surface **11a**) shown in FIGS. **1** and **3**. The holding surface **11a** includes a first region **S₁** and a second region **S₂** each of which includes a plurality of sample liquid chip mount portions. (For clarity, the boundary between the first region **S₁** and the second region **S₂** is indicated by a phantom line in FIG. **3**.) In this embodiment, the maximum number of sample liquid chips **40** that can be held in the first region **S₁** and the maximum number of sample liquid chips **40** that can be held in the second region **S₂** are equal to each other. In this embodiment, the sample liquid chips **40** are held on the holding surface **11a** as arranged on an imaginary circle around the axis **Ax**.

The specific structure of each sample liquid chip **40** is shown in FIGS. **5A** and **5B**. FIG. **5A** is an enlarged plan view of the sample liquid chip **40**. FIG. **5B** is a sectional view taken along lines V-V in FIG. **5A**. The sample liquid chip **40** is provided by bonding a main body **41** having a recess and a cover **42** having an opening. The sample liquid chip **40** includes a sample liquid cell **43** defined between cell walls **41a** and **42a** facing and spaced from each other, a liquid retaining space **44** communicating with the sample liquid cell **43**, and an introduction port **45** provided at a position corresponding to the liquid retaining space **44**. The main body **41** and the cover **42** can be made by resin molding. Examples of resin material for making the main body **41** and the cover **42** include PS, PC, PMMA, COC and COP. The cell wall **41a** is part of the main body **41**, whereas the cell wall **42a** is part of the cover **42**. The thickness of the cell wall **41a**, **42a** (the thickness shown in FIG. **5B**) is e.g. 10 to 500 μm . The sample liquid cell **43** is a space for receiving a predetermined sample liquid or the like for performing the PCR method (not shown in FIGS. **5A** and **5B**). The sample liquid cell **43** is shallow. Specifically, the maximum dimension of the sample liquid cell **43** in a direction perpendicular to the spacing direction of the cell walls **41a** and **42a** (e.g. 1000 μm) is larger than the maximum dimension of the sample liquid cell **43** in the spacing direction (e.g. 500 μm). The volume of the sample liquid cell **43** is e.g. 0.1 to 100 μL . A sample liquid containing template DNA, primer DNA, DNA polymerase, and dNTP is introduced into the sample liquid cell **43**. The liquid retaining space **44** is a space for preparing the sample liquid to be introduced into the sample liquid cell **43** by mixing various kinds of reagents or the like. The introduction port **45** is used for supplying various kinds of reagents or the like into the liquid retaining space **44**.

As shown in FIG. **3**, in mounting a sample liquid chip **40** onto the holding surface **11a** (which is rotatable), the sample liquid chip **40** is arranged in a sample liquid chip mount portion such that the sample liquid cell **43** is positioned on a radially outer side of the holding surface **11a** and the liquid retaining space **44** is positioned on a radially inner side of the holding surface **11a**. The sample liquid chip **40** is removably mounted to the holding surface **11a** of the rotation table **11**. Specifically, for instance, a plurality of recesses (now shown) may be formed on a side of the sample liquid chip **40** that is to come into contact with the holding surface **11a** (i.e., the main body **41** side), whereas a plurality of projections (not shown) for fitting into the recesses may be formed on the holding surface **11a** in each of the sample liquid chip mount portions at locations corresponding to the recesses. Further, a clipping mechanism for clipping the sample liquid chip **40** onto the holding surface **11a**, with the above-described projections fitted in the above-described recesses, may be provided at each sample liquid chip mount portion. By employing this

structure in the temperature controlling unit **X1**, each of the sample liquid chips **40** can be removably held at a predetermined position in the holding surface **11a** of the rotation table **11**. When the sample liquid chips **40** are held on the holding surface **11a** of the rotation table **11**, the holding surface **11a** comes into contact with the main body **41** side (including the cell wall **41a**) of each sample liquid chip **40**.

A temperature sensor **11b** for detecting the temperature of the holding surface **11a** is provided on the holding surface **11a** or inside the rotation table **11** adjacent to the holding surface **11a**. For instance, the temperature sensor **11b** comprises a thermistor. As shown in FIG. **2**, the temperature sensor **11b** is connected to the microcomputer MC. Signals outputted from the temperature sensor **11b** are inputted into the microcomputer MC.

The temperature control device **21** (not shown in FIG. **1**) is arranged in the rotation table **11**. The temperature control device **21** is thermally connected to the holding surface **11a** of the rotation table **11**. The temperature control device **21** comprises a Peltier module that utilizes Peltier effect. As shown in FIG. **2**, the temperature control device **21** is connected to the microcomputer MC. The amount and direction of electric current to be applied to the Peltier module (temperature control device **21**) is changed as required in accordance with the instructions from the microcomputer MC. By the operation of the temperature control device **21**, the rotation table **11** or at least the holding surface **11a** of the rotation table is kept at a first temperature **T₁**. The first temperature **T₁** is a temperature for keeping the sample liquid in the sample liquid chips **40** on the holding surface **11a** at a lower target temperature **T_L**. The first temperature **T₁** is set appropriately depending on the lower target temperature **T_L** for the sample liquid as a target for temperature control, environmental temperature, thermal conductivity of the material for the sample liquid chips **40** and the structure and heat dissipation ability of the sample liquid chips **40**, for example. For instance, when the lower target temperature **T_L** is equal or substantially equal to the environmental temperature, it may be suitable to set the first temperature **T₁** to be equal to the lower target temperature **T_L**. For instance, when the lower target temperature **T_L** is considerably higher than the environmental temperature, it may be suitable to set the first temperature **T₁** to be higher than the lower target temperature **T_L**. For instance, when the lower target temperature **T_L** is considerably lower than the environmental temperature, it may be suitable to set the first temperature **T₁** to be lower than the lower target temperature **T_L**.

The driving mechanism **31** drives the rotation table **11** for rotation. The driving mechanism **31** is connected to the microcomputer MC and operates in accordance with the instructions from the microcomputer MC. The driving mechanism **31** outputs the amount of rotation of the rotation table **11** to the microcomputer MC. The rotation table **11** is fixed to the rotation shaft of the driving mechanism **31**.

The heating block **12** is designed to come into contact with the sample liquid chips **40** to heat the sample liquid in the sample liquid cells **43** of the sample liquid chips **40**. The heating block **12** is movable relative to the sample liquid chips **40** on the holding surface **11a**. Specifically, the heating block **12** faces the holding surface **11a** of the rotation table **11** and is movable toward and away from the holding surface **11a** or the sample liquid chips **40** on the holding surface **11a** in the arrow H direction shown in FIG. **1**. The heating block **12** is kept at a second temperature **T₂** higher than a higher target temperature **T_H** (that is higher than the above-described lower target temperature **T_L**) for the sample liquid as a target for temperature control. As shown in FIGS. **1** and **4**, the heating block **12** has a plurality of projections **12a**. Each of the projections **12a**

is arranged to come into contact with the cell wall **42a** of the sample liquid chip **40** on the holding surface **11a** (i.e., the side of the sample liquid chip **40** opposite from the rotation table **11**).

A temperature sensor **12b** for detecting the temperature of the heating block **12** is provided in the heating block **12**. For instance, the temperature sensor **12b** comprises a thermistor. As shown in FIG. 2, the temperature sensor **12b** is connected to the microcomputer MC. Signals outputted from the temperature sensor **12b** are inputted into the microcomputer MC.

The temperature control device **22** (not shown in FIG. 1) is thermally connected to the heating block **12**. The temperature control device **22** is a heater comprising a heating device. The amount of electric current to be applied to the temperature control device **22** is changed as required in accordance with the instructions from the microcomputer MC, whereby the temperature of the temperature control device **22** changes. By the operation of the temperature control device **22**, the heating block **12** is kept at the second temperature T_2 .

The driving mechanism **32** (not shown in FIG. 1) drives the heating block **12** for translation in the arrow H direction shown in FIG. 1. As shown in FIG. 2, the driving mechanism **32** is connected to the microcomputer MC. The driving mechanism **32** operates in accordance with the instructions from the microcomputer MC and outputs the amount of translation of the heating block **12** to the microcomputer MC. By the operation of the driving mechanism **32**, the heating block **12** moves toward and away from the holding surface **11a** of the rotation table **11**.

The cooling block **13** is designed to come into contact with the sample liquid chips **40** to cool the sample liquid in the sample liquid cells **43** of the sample liquid chips **40**. The cooling block **13** is movable relative to the sample liquid chips **40** on the holding surface **11a**. Specifically, the cooling block **13** faces the holding surface **11a** of the rotation table **11** and is movable toward and away from the holding surface **11a** or the sample liquid chips **40** on the holding surface **11a**. The cooling block **13** is kept at a third temperature T_3 lower than the lower target temperature T_L for the sample liquid as a target for temperature control. The third temperature T_3 , which is lower than the lower target temperature T_L , is lower than the first temperature T_1 as well. As shown in FIGS. 1 and 4, the cooling block **13** has a plurality of projections **13a**. Each of the projections **13a** is arranged to come into contact with the cell wall **42a** of the sample liquid chip **40** on the holding surface **11a** (i.e., the side of the sample liquid chip **40** opposite from the rotation table **11**).

A temperature sensor **13b** for detecting the temperature of the cooling block **13** is provided in the cooling block **13**. For instance, the temperature sensor **13b** comprises a thermistor. As shown in FIG. 2, the temperature sensor **13b** is connected to the microcomputer MC. Signals outputted from the temperature sensor **13b** are inputted into the microcomputer MC.

The temperature control device **23** (not shown in FIG. 1) is thermally connected to the cooling block **13**. The temperature control device **23** comprises a Peltier module that utilizes Peltier effect. As shown in FIG. 2, the temperature control device **23** is connected to the microcomputer MC. The amount and direction of electric current to be applied to the Peltier module (temperature control device **23**) is changed as required in accordance with the instructions from the microcomputer MC. By the operation of the temperature control device **23**, the cooling block **13** is kept at the third temperature T_3 .

The driving mechanism **33** (not shown in FIG. 1) drives the cooling block **13** for translation in the arrow H direction shown in FIG. 1. As shown in FIG. 2, the driving mechanism

33 is connected to the microcomputer MC. The driving mechanism **33** operates in accordance with the instructions from the microcomputer MC and outputs the amount of translation of the cooling block **13** to the microcomputer MC. By the operation of the driving mechanism **33**, the cooling block **13** moves toward and away from the holding surface **11a** of the rotation table **11**.

To perform the PCR method in the temperature controlling unit X1, sample liquid chips **40** are mounted on the holding surface **11a** of the rotation table **11** and then sample liquid is introduced into the sample liquid chips **40** in the following manner, for example.

First, as shown in FIG. 3, for example, a necessary number of sample liquid chips **40** are set on the sample liquid chip mount portions in the holding surface **11a** of the rotation table **11**. (As described above, in this process, each of the sample liquid chips **40** is arranged such that the sample liquid cell **43** is positioned on a radially outer side of the holding surface **11a** and the liquid retaining space **44** is positioned on a radially inner side of the holding surface.) The position of each of the sample liquid chips **40** on the holding surface **11a** is fixed during the subsequent steps. Then, as shown in FIG. 6A, necessary reagents or the like are introduced into the liquid retaining space **44** through the introduction port **45**. Specifically, for example, each reagent may be prepared in the form of a solution and supplied into the liquid retaining space **44**. Alternatively, part of the reagents may be prepared in the form of a dried reagent and applied in advance to the bottom surface of the liquid retaining space **44**. In this case, other reagents each prepared as a solution are then supplied into the liquid retaining space **44** so that the dried reagent dissolves into the reagents in the form of a solution. Examples of necessary reagents or the like include template DNA, primer DNA, DNA polymerase, dNTP and a buffer component. The reagents are mixed within the liquid retaining space **44** by e.g. pipetting, whereby a sample liquid **50** as a homogenous reaction liquid is obtained. Then, the rotation table **11** is rotated about the axis Ax at a predetermined speed. The centrifugal force acting on the sample liquid **50** due to the rotation of the rotation table **11** causes the sample liquid **50** to move into the sample liquid cell **43**, as shown in FIG. 6B. Then, as shown in FIG. 6C, mineral oil **60** is supplied into the liquid retaining space **44**. The presence of mineral oil **60** prevents the sample liquid **50** from being lost by evaporation, for example, in the subsequent temperature change process.

Then, the rotation table **11** is fixed at a predetermined rotational position about the axis Ax. Specifically, by the operation of the driving mechanism **31**, the position of the rotation table **11** is fixed such that the first region S_1 of the holding surface **11a** faces the heating block **12** whereas the second region S_2 of the holding surface **11a** faces the cooling block **13**.

Then, each of the rotation table **11**, the heating block **12** and the cooling block **13** is set to a desired temperature and kept at the desired temperature. Specifically, this process is performed in the following manner. The temperature of the rotation table **11** at least at the holding surface **11a** is adjusted to the above-described first temperature T_1 by the operation of the temperature control device **21**, and the first temperature T_1 is maintained. The temperature of the heating block **12** is adjusted to the above-described second temperature T_2 (heating temperature) by the operation of the temperature control device **22**, and the second temperature T_2 is maintained. The temperature of the cooling block **13** is adjusted to the above-described third temperature T_3 (cooling temperature) by the operation of the temperature control device **23**, and the third temperature T_3 is maintained. The lower target temperature

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which the sample liquid 50 should reach in the PCR process is expressed as T_L (e.g. 60° C.), whereas the higher target temperature which the sample liquid should reach in the PCR process is expressed as T_H (e.g. 95° C.). In such a case, the first temperature T_1 is a temperature by which the temperature of the sample liquid 50 can be kept at the lower target temperature T_L when a sufficient time has elapsed in a state where no heat transfer occurs from the heating block 12 to the sample liquid 50 and no heat transfer from the sample liquid 50 to the cooling block 13. Specifically, the first temperature T_1 may be a temperature equal to the lower target temperature T_L , or a temperature higher than the lower target temperature T_L and lower than the higher target temperature T_H , or a temperature lower than the lower target temperature T_L and higher than the third temperature T_3 (cooling temperature). The second temperature T_2 is a temperature higher than the higher target temperature T_H . The third temperature T_3 is a temperature lower than the lower target temperature T_L .

In the temperature controlling unit X1, after the preparation as described above is completed and the temperature of the sample liquid 50 has reached the lower target temperature T_L , the PCR method or temperature control is performed in a parallel manner. In this parallel PCR method, the temperature increase step, the temperature reduction step and the temperature maintaining step are performed with respect to the sample liquid 50 in the sample liquid chips 40 held in the first region S_1 (constituting the first group) of the holding surface 11a, while at the same time, the temperature increase step, the temperature reduction step and the temperature maintaining step are performed with respect to the sample liquid 50 in the sample liquid chips 40 held in the second region S_2 (constituting the second group) of the holding surface 11a. FIG. 7 shows part of a table of steps in the temperature control performed by the temperature controlling unit X1.

First, in the parallel PCR method by the temperature controlling unit X1, the temperature increase step is performed in Step 1 with respect to the sample liquid chips 40 held in the first region S_1 , as shown in FIG. 8. (For clarity, the first region S_1 side of the rotation table 11 is hatched in FIG. 8 and FIGS. 9-12 as well.)

Specifically, in Step 1, the heating block 12 is moved closer to the rotation table 11 to come into contact with the sample liquid chips 40 in the first region S_1 of the holding surface 11a by the operation of the driving mechanism 32, as shown in FIG. 8. More specifically, as shown in FIG. 13, each projection 12a of the heating block 12 is brought into contact with the cell wall 42a of the corresponding sample liquid chip 40. (The cell wall 42a, along with the cell wall 41a, defines the sample liquid cell 43.) By this contact, the temperature increase step with respect to the sample liquid chips 40 of the first group is started. In this temperature increase step, the cell wall 42a of the sample liquid chip 40 is directly heated by the heating block 12 or the projection 12a. By heating the cell wall 42a, heat transfers from the heating block 12 or the projection 12a to the cell wall 42a and the sample liquid 50 in the sample liquid cell 43. Thus, the temperature of the sample liquid 50 increases and reaches the higher target temperature T_H . As a result, the two strands of a template DNA in the sample liquid 50 are sufficiently separated from each other (the thermal denaturation step of the first group). When the sample liquid 50 reaches the higher target temperature T_H , the heating block 12 or the projection 12a is separated from the cell wall 42a of the sample liquid chip 40. Thus, heat transfer from the heating block 12 to the sample liquid 50 stops (end of the temperature increase step of the first group).

In Step 1, on the other hand, the sample liquid 50 in the sample liquid chips 40 in the second region S_2 (the second

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group) are kept at a constant temperature (lower target temperature T_L) and in a standby state. Any reaction related to PCR does not occur in the sample liquid 50 in these sample liquid chips 40 of the second group.

When Step 1 is finished, the heating block 12 is separated from the sample liquid chips 40 of the first group as described above, and at the same time, the rotation table 11 is rotated 180° about the axis Ax by the operation of the driving mechanism 31. Due to this rotation, the position of the sample liquid chips 40 in the first region S_1 that belong to the first group switches with the position of the sample liquid chips 40 in the second region S_2 that belong to the second group.

Next, in Step 2, the temperature reduction step is performed with respect to first group, whereas the temperature increase step is performed with respect to the second group, as shown in FIG. 9.

Specifically, in Step 2, the cooling block 13 is moved closer to the rotation table 11 to come into contact with the sample liquid chips 40 in the first region S_1 of the holding surface 11a by the operation of the driving mechanism 33, as shown in FIG. 9. More specifically, as shown in FIG. 14, each projection 13a of the cooling block 13 is brought into contact with the cell wall 42a of the corresponding sample liquid chip 40. (The cell wall 42a, along with the cell wall 41a, defines the sample liquid cell 43.) By this contact, the temperature reduction step with respect to the sample liquid chips 40 of the first group is started. In this temperature reduction step, the cell wall 42a of the sample liquid chip 40 is directly cooled by the cooling block 13 or the projection 13a. Heat transfers from the cell wall 42a and the sample liquid 50 in the sample liquid cell 43 to the cooling block 13 or the projection 13a. Thus, the temperature of the sample liquid 50 reduces. During the temperature reduction, annealing gradually proceeds within the sample liquid 50 (part of the annealing step of the first group). In this annealing step, each single-stranded DNA of the template combines with a primer (containing a base sequence complementary to part of the single-stranded DNA). The cooling block 13 or the projection 13a is separated from the cell wall 42a of the sample liquid chip 40 by the operation of the driving mechanism 33 immediately before (e.g. 10 to 1000 milliseconds before) the sample liquid 50 reaches the lower target temperature T_L . Thus, heat transfer to the cooling block 13 stops (end of the temperature reduction step of the first group; end of Step 2).

In Step 2, on the other hand, the heating block 12 is moved closer to the rotation table 11 to come into contact with the sample liquid chips 40 in the second region S_2 of the holding surface 11a by the operation of the driving mechanism 32, as shown in FIG. 9. More specifically, as shown in FIG. 13, each projection 12a of the heating block 12 is brought into contact with the cell wall 42a of the corresponding sample liquid chip 40. By this contact, the temperature increase step with respect to the sample liquid chips 40 of the second group is started. In this temperature increase step, the cell wall 42a of the sample liquid chip 40 is directly heated by the heating block 12 or the projection 12a. Heat transfers from the heating block 12 or the projection 12a to the cell wall 42a and the sample liquid 50 in the sample liquid cell 43. Thus, the temperature of the sample liquid 50 increases.

Next, in Step 3, the temperature maintaining step is performed with respect to the first group, whereas the temperature increase step is performed continuously from Step 2 with respect to the second group, as shown in FIG. 10.

In Step 3, the sample liquid chips 40 of the first group are left in contact with the holding surface 11a and the sample liquid 50 in each of the sample liquid chips 40 is kept at a constant temperature (the lower target temperature T_L) (the

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temperature maintaining step of the first group). In the sample liquid **50** in this state, annealing (part of the annealing step of the first group) and elongation (part of the elongation step of the first group) proceed at the same time. In the annealing step, as described above, each single-stranded DNA of the template combines with a primer (containing a base sequence complementary to part of the single-stranded DNA). In the elongation step, at the 3' end of the primer combined with the single-stranded DNA of the template, a DNA strand containing base sequence complementary to single-stranded DNA is elongated or synthesized.

In Step 3, continuously from Step 2, the cell wall **42a** of each sample liquid chip **40** of the second group is directly heated by the heating block **12** or the projection **12a**, and heat transfers from the heating block **12** or the projection **12a** to the cell wall **42a** and the sample liquid **50** in the sample liquid cell **43**. When the sample liquid **50** reaches the higher target temperature T_H , the two strands of a template DNA in the sample liquid **50** are sufficiently separated from each other (thermal denaturation step of the second group). When the sample liquid **50** reaches the higher target temperature T_H , the heating block **12** or the projection **12a** is separated from the cell wall **42a** of the sample liquid chip **40** by the operation of the driving mechanism **32**. Thus, heat transfer from the heating block **12** to the sample liquid **50** stops (end of the temperature increase step of the first group).

When Step 3 is finished, the heating block **12** is separated from the sample liquid chips **40** of the second group as described above, and at the same time, the rotation table **11** is rotated 180° about the axis Ax by the operation of the driving mechanism **31**. Due to this rotation, the position of the sample liquid chips **40** in the first region S_1 that belong to the first group switches with the position of the sample liquid chips **40** in the second region S_2 that belong to the second group.

Next, in Step 4, the temperature maintaining step is performed continuously from Step 3 with respect to the first group, whereas the temperature reduction step is performed with respect to the second group, as shown in FIG. 11.

In Step 4, continuously from Step 3, the sample liquid chips **40** of the first group are left in contact with the holding surface **11a** and the sample liquid **50** in the sample liquid cell **43** of each of the sample liquid chips **40** is kept at a constant temperature (the lower target temperature T_L). Thus, in the sample liquid **50** of the first group, continuously from Step 3, annealing (part of the annealing step of the first group) and elongation (part of the elongation step of the first group) proceed at the same time.

In Step 4, the cooling block **13** is moved closer to the rotation table **11** to come into contact with the sample liquid chips **40** in the second region S_2 of the holding surface **11a** by the operation of the driving mechanism **33**, as shown in FIG. 11. More specifically, as shown in FIG. 14, each projection **13a** of the cooling block **13** is brought into contact with the cell wall **42a** of the corresponding sample liquid chip **40**. By this contact, the temperature reduction step with respect to the sample liquid chips **40** of the second group is started. In this temperature reduction step, the cell wall **42a** of the sample liquid chip **40** is directly cooled by the cooling block **13** or the projection **13a**. Heat transfers from the cell wall **42a** and the sample liquid **50** in the sample liquid cell **43** to the cooling block **13** or the projection **13a**. Thus, the temperature of the sample liquid **50** reduces. During the temperature reduction, annealing gradually proceeds within the sample liquid **50** (part of the annealing process of the second group). The cooling block **13** or the projection **13a** is separated from the cell wall **42a** of the sample liquid chip **40** by the operation of the driving mechanism **33** immediately before (e.g. 10 to

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1000 milliseconds before) the sample liquid **50** reaches the lower target temperature T_L . Thus, the heat transfer to the cooling block **13** stops (end of the temperature reduction step of the second group; end of Step 4).

Next, in Step 5, the temperature maintaining step is performed continuously from Step 4 with respect to the first group, and the temperature maintaining step is performed with respect to the second group as well, as shown in FIG. 12.

In Step 5, continuously from Step 4, the sample liquid chips **40** of the first group are left in contact with the holding surface **11a** and the sample liquid **50** in the sample liquid cell **43** of each of the sample liquid chips **40** is kept at a constant temperature (the lower target temperature T_L). Thus, in the sample liquid **50** of the first group, continuously from Step 4, annealing (part of the annealing step of the first group) and elongation (part of the elongation step of the first group) proceed at the same time.

In Step 5, the sample liquid chips **40** of the second group are left in contact with the holding surface **11a** and the sample liquid **50** in the sample liquid cell **43** of each of the sample liquid chips **40** is kept at a constant temperature (the lower target temperature T_L) (the temperature maintaining step of the second group). Thus, in the sample liquid **50**, annealing (part of the annealing step of the second group) and elongation (part of the elongation step of the second group) proceed at the same time.

Next, in Step 6, the temperature increase step (of the second cycle) is performed with respect to the first group, whereas the temperature maintaining step is performed continuously from Step 5 with respect to the second group, as shown in FIG. 8.

In Step 6, the temperature increase step is performed with respect to the sample liquid chips **40** of the first group in the first region S_1 , similarly to the temperature increase step described above with respect to Step 1. Meanwhile, the sample liquid chips **40** of the second group in the second region S_2 are left in contact with the holding surface **11a** and the sample liquid **50** in the sample liquid cell **43** of each of the sample liquid chips **40** is kept at a constant temperature (the lower target temperature T_L). Thus, in the sample liquid **50** of the second group, annealing (part of the annealing step of the second group) and elongation (part of the elongation step of the second group) proceed at the same time, continuously from Step 5. The temperature maintaining step of the second group is completed when Step 6 is finished.

When Step 6 is finished, the heating block **12** is separated from the sample liquid chips **40** of the first group in the first region S_1 , and at the same time, the rotation table **11** is rotated 180° about the axis Ax by the operation of the driving mechanism **31**. Due to this rotation, the position of the sample liquid chips **40** in the first region S_1 that belong to the first group switches with the position of the sample liquid chips **40** in the second region S_2 that belong to the second group.

As to Steps 1-6 described above, the temperature increase step of the first group in Step 1 is performed for e.g. six seconds, the temperature reduction step of the first group in Step 2 is performed for e.g. four seconds, and the temperature maintaining step of the first group through Steps 3-5 is performed for e.g. 16 seconds. (The temperature increase step of the first group in Step 6 is performed for the same period of time as that in Step 1.) The temperature increase step of the second group through Steps 2-3 is performed for e.g. six seconds, the temperature reduction step of the second group in Step 4 is performed for e.g. four seconds, and the temperature maintaining step of the second group through Steps 5-6 is performed for e.g. 16 seconds.

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In the temperature controlling unit X1, a thermal cycle consisting of the above-described Steps 1-5 is performed repetitively with respect to the sample liquid 50 in the sample liquid cells 43 of the sample liquid chips 40 in the first region S₁ (first group). Thus, the PCR method that repeats a cycle including thermal denaturation, annealing and elongation a predetermined number of times can be performed. In parallel with this, in the temperature controlling unit X1, a thermal cycle consisting of the above-described Steps 2-6 is performed repetitively with respect to the sample liquid 50 in the sample liquid cells 43 of the sample liquid chips 40 in the second region S₂ (second group). Thus, the PCR method that repeats a cycle including thermal denaturation, annealing and elongation a predetermined number of times can be performed also with respect to the sample liquid 50 in the sample liquid cells 43 of the sample liquid chips 40 of the second group. In this way, in the temperature controlling unit X1, the PCR method or the temperature control is performed in a parallel manner.

The temperature controlling unit X1 that operates as described above is suitable for quickly changing the temperature of the sample liquid. The reason is as follows.

The temperature controlling unit X1 is designed such that the heating block 12 can come into direct contact with the cell wall 42a of the sample liquid cell 43 to increase the temperature of the sample liquid 50. Thus, in the temperature increase step, the heating block 12 heats the sample liquid 50 in direct contact with the cell wall 42a. In the above-described conventional PCR machine X2, for example, the heating block 92 needs to heat the tube 94 or the reaction sample liquid in the tube via the holding block 91 (heat capacity member) that holds the tube 94, and the holding block 91 has a large heat capacity. Thus, in the PCR machine X2, to increase the temperature of the reaction sample liquid in the tube 94 to the higher target temperature, it is necessary to increase the temperature of the holding block 91 as well, which has a large heat capacity, to the higher target temperature. Thus, the holding block 91 (heat capacity member) tends to hinder quick temperature increase of the reaction sample liquid. In the temperature increase step by the temperature controlling unit X1, on the other hand, it is not necessary to heat the sample liquid chip 40 or the sample liquid 50 via a heat capacity member for holding the sample liquid chip 40. Thus, the temperature controlling unit X1, in which no member having a large heat capacity intervenes between the heating block 12 and the sample liquid chip 40 or the sample liquid 50, is suitable for quickly increasing the temperature of the sample liquid 50 in the sample liquid cell 43.

With respect to the temperature controlling unit X1, it is supposed that the temperature of the sample liquid 50 in the sample liquid cell 43 during the temperature increase step is represented by T, the amount of heat supplied to the sample liquid 50 is represented by Q, and time is represented by t. Now, the increasing rate of the temperature, i.e., the temperature increase speed of the sample liquid 50 in the temperature increase step (dT/dt) is proportional to the amount of heat supplied to the sample liquid 50 per unit time (dQ/dt). The amount of heat supplied to the sample liquid 50 per unit time (dQ/dt) is highly related to the temperature difference (T₂-T) between the sample liquid 50 and the heating block 12 (kept at a second temperature T₂ higher than the higher target temperature T_H) and is substantially proportional to the temperature difference (T₂-T). A larger temperature difference (T₂-T) leads to a larger amount of heat supply to the sample liquid 50 per unit time (dQ/dt) and also to a higher temperature increase speed (dT/dt). In the conventional PCR machine X2, the temperature of the heating block 92 is kept at the thermal

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denaturation temperature T₁₁ that is the higher target temperature of the reaction sample liquid, and thus the difference from the temperature T of the reaction sample liquid during the temperature increase step is (T₁₁-T). As will be understood by comparing the temperature controlling unit X1 and the conventional PCR machine X2 on the assumption that the higher target temperatures are equal (i.e., T_H=T₁₁), the temperature difference (T₂-T) between the sample liquid 50 and the heating block 12 in the temperature controlling unit X1 can be larger than the temperature difference (T₁₁-T) between the reaction sample liquid and the heating block 92 in the PCR machine X2 (T₂>T_H=T₁₁). As noted before, a larger temperature difference (T₂-T) leads to a larger amount of heat supply to the sample liquid 50 per unit time (dQ/dt). Accordingly, the temperature increase speed (dT/dt) of the sample liquid 50 is high.

In the temperature increase step with the temperature controlling unit X1, the temperature increase speed (dT/dt) can be made advantageously high in a temperature range close to the higher target temperature T_H. As described with reference to FIG. 20, according to the conventional PCR machine X2, the temperature increase speed in a temperature range close to the thermal denaturation temperature T₁₁ (higher target temperature) in the temperature increase step is considerably low as compared with the temperature increase speed in the initial stage of the temperature increase step. This is because, as the temperature T of the reaction sample liquid increases to approach the thermal denaturation temperature T₁₁ (the higher target temperature), the temperature difference (T₁₁-T) between the reaction sample liquid and the heating block 92 becomes considerably small. (A smaller temperature difference leads to a smaller amount of heat supply to the reaction sample liquid per unit time and hence to a lower temperature increase speed.) On the other hand, according to the temperature controlling unit X1, the temperature difference (T₂-T) between the sample liquid 50 and heating block 12 during temperature increase can be made considerably large even in a temperature range close to the higher target temperature T_H in the temperature increase step. Thus, the amount of heat supply to the sample liquid 50 in the sample liquid cell 43 per unit time (dQ/dt) can be made large. Thus, according to the temperature controlling unit X1, the temperature increase speed (dT/dt) in a temperature range close to the higher target temperature T_H in the temperature increase step can be made large.

Further, the temperature controlling unit X1 is designed such that the cooling block 13 can come into direct contact with the cell wall 42a of the sample liquid cell 43 to reduce the temperature of the sample liquid 50. Thus, in the temperature reduction step, the cooling block 13 cools the sample liquid 50 in direct contact with the cell wall 42a. In the above-described conventional PCR machine X2, for example, the cooling block 93 needs cool the tube 94 or the reaction sample liquid in the tube via a holding block 91 (heat capacity member) holding the tube 94, and the holding block 91 has a large heat capacity. Thus, in the PCR machine X2, to reduce the temperature of the reaction sample liquid in the tube 94 to the lower target temperature, it is necessary to reduce the temperature of the holding block 91 as well, which has a large heat capacity, to the lower target temperature. Thus, the holding block 91 (heat capacity member) tends to hinder quick temperature reduction of the reaction sample liquid. In the temperature reduction step by the temperature controlling unit X1, on the other hand, the cooling of the sample liquid chip 40 or the sample liquid 50 can be conducted with no intervention of a heat capacity member for holding the sample liquid chip 40. Thus, the temperature controlling unit X1, in

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which no large heat capacity member intervenes between the cooling block **13** and the sample liquid chip **40** or the sample liquid **50**, is suitable for quickly reducing the temperature of the sample liquid **50** in the sample liquid cell **43**.

With respect to the temperature controlling unit **X1**, it is supposed that the temperature of the sample liquid **50** in the sample liquid cell **43** during the temperature reduction step is represented by T , the amount of heat taken from the sample liquid **50** is represented by Q , and time is represented by t . The reducing rate of the temperature, i.e., the temperature reduction speed of the sample liquid **50** in the temperature reduction step ($-dT/dt$) is proportional to the amount of heat taken from the sample liquid **50** per unit time (dQ/dt). The amount of heat taken from the sample liquid per unit time (dQ/dt) is highly related to the temperature difference ($T-T_3$) between the sample liquid **50** which is the target to be cooled and the cooling block **13** (kept at a third temperature T_3 lower than the lower target temperature T_L) and is substantially proportional to the temperature difference ($T-T_3$). A larger temperature difference ($T-T_3$) leads to a larger amount of heat taken from the sample liquid per unit time (dQ/dt) and also to a higher temperature reduction speed ($-dT/dt$). In the conventional PCR machine **X2**, the temperature of the cooling block **93** is kept at the annealing/elongation temperature T_{12} that is the lower target temperature of the reaction sample liquid, and thus the difference from the temperature T of the reaction sample liquid during the temperature reduction step is ($T-T_{12}$). As will be understood by comparing the temperature controlling unit **X1** and the conventional PCR machine **X2** on the assumption that the lower target temperatures are equal (i.e., $T_L=T_{12}$), the temperature difference ($T-T_3$) between the sample liquid **50** and the cooling block **13** in the temperature controlling unit **X1** can be made larger than the temperature difference ($T-T_{12}$) between the reaction sample liquid and the cooling block **93** in the PCR machine **X2** ($T_3 < T_L = T_{12}$). As noted before, a larger temperature difference ($T-T_3$) leads to a larger amount of heat taken from the sample liquid **50** in the sample liquid cell **43** per unit time (dQ/dt). Thus, the temperature reduction speed ($-dT/dt$) of the sample liquid **50** is high.

In the temperature controlling unit **X1**, the temperature reduction speed ($-dT/dt$) can be made advantageously high in a temperature range close to the lower target temperature T_L . As described with reference to FIG. **20**, according to the conventional PCR machine **X2**, the temperature reduction speed in the temperature reduction step in a temperature range close to the annealing/elongation temperature T_{12} (lower target temperature) is considerably low as compared with the temperature reduction speed in the initial stage of the temperature reduction step. This is because, as the temperature T of the reaction sample liquid reduces to approach the annealing/elongation temperature T_{12} (the lower target temperature), the temperature difference ($T-T_{12}$) between the reaction sample liquid and the cooling block **93** becomes considerably small. (A smaller temperature difference leads to a smaller amount of heat taken from the reaction sample liquid per unit time and hence to a lower temperature reduction speed.) On the other hand, according to the temperature controlling unit **X1**, the temperature difference ($T-T_3$) between the sample liquid **50** and cooling block **13** during the temperature reduction can be made considerably large even in a temperature range close to the lower target temperature T_L in the temperature reduction step. Thus, the amount of heat taken from the sample liquid **50** in the sample liquid cell **43** per unit time (dQ/dt) can be made large. Thus, according to the temperature controlling unit **X1**, the temperature reduc-

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tion speed ($-dT/dt$) in a temperature range close to the lower target temperature T_L in the temperature reduction step can be made large.

As described above, the temperature controlling unit **X1** is suitable for quickly changing (increasing or reducing) the temperature of the sample liquid **50**. Although the temperature controlling unit **X1** is suitable for use as a PCR machine, which requires quick temperature control, the temperature controlling unit can be used also as other kinds of temperature controlling unit.

Moreover, the temperature controlling unit **X1** is suitable for controlling the temperature of the sample liquid **50** precisely to the higher target temperature T_H or the lower target temperature T_L . The reason is as follows.

In theory, in the conventional PCR machine **X2**, as the temperature of the reaction sample liquid T approaches the thermal denaturation temperature T_{11} , the reaction sample liquid temperature T and the temperature T_{11} of the heating block **92** become closer to each other, and the temperature increase speed (dT/dt) of the reaction sample liquid, which is substantially proportional to the temperature difference ($T_{11}-T$), approaches 0. Thus, in theory, in the conventional PCR machine **X2**, the reaction sample liquid temperature T cannot reach the thermal denaturation temperature T_{11} (higher target temperature) within a finite time in the temperature increase step. In practice as well, in the conventional PCR machine **X2**, the reaction sample liquid temperature T hardly reaches the thermal denaturation temperature T_{11} in the temperature increase step. Thus, it is difficult to cause the reaction sample liquid temperature T to reach the precise thermal denaturation temperature T_{11} . In contrast, in the temperature controlling unit **X1**, the temperature increase speed (dT/dt) of the sample liquid **50** can be made high in a temperature range close to the higher target temperature T_H in the temperature increase step, as described above. This means that the temperature increase speed (dT/dt) of the sample liquid **50** can be kept high until the temperature T of the sample liquid **50** reaches the higher target temperature T_H so that the temperature T of the sample liquid **50** reaches the higher target temperature T_H quickly and reliably. By separating the heating block **12** from the sample liquid chip **40** when the temperature T of the sample liquid **50** in the sample liquid chip **40** has reached the higher target temperature T_H , heat transfer from the heating block **12** to the sample liquid chip **40** or the sample liquid **50** can be stopped, whereby temperature increase of the sample liquid **50** can be stopped. The temperature controlling unit **X1** having such a structure is suitable for controlling the temperature T of the sample liquid **50** precisely to the higher target temperature T_H .

Generally, in reducing the temperature of a liquid by continuously taking heat from the liquid, the temperature of the liquid sometimes continues to drop even after the taking of heat from the liquid is stopped. For instance, in the above-described temperature reduction step of the conventional PCR machine **X2**, the cooling block **93** is separated from the holding block **91** to stop taking heat from the reaction sample liquid when the reaction sample liquid temperature T reaches the annealing/elongation temperature T_{12} (the lower target temperature). However, even after this, the reaction sample liquid temperature sometimes continues to drop below the annealing/elongation temperature T_{12} . Thus, with the conventional PCR machine **X2**, it is difficult to control the reaction sample liquid temperature T precisely to the annealing/elongation temperature T_{12} . In the temperature controlling unit **X1**, the rotation table **11** holds the sample liquid chip **40** in contact with the cell wall **41a** of the sample liquid cell **43** of the sample liquid chip **40**. (The temperature of the rotation

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table 11 is set to and kept at the first temperature T_1 for keeping the sample liquid 50 at the lower target temperature T_L . This prevents the temperature T of the sample liquid 50 from continuing to drop after the separation of the cooling block 13 from the cell wall 42a. The temperature controlling unit X1 having this arrangement is suitable for controlling the temperature T of the sample liquid 50 in the temperature reduction step precisely to the lower target temperature T_L .

As described above, the temperature controlling unit X1 is suitable for controlling the sample liquid 50 precisely to the higher target temperature T_H or the lower target temperature T_L . Although this temperature controlling unit X1 is suitable for use as a PCR machine, which requires precise temperature control, the temperature controlling unit can be used also as other kinds of temperature controlling unit.

As noted before, in the temperature controlling unit X1, the heating block 12 and the cooling block 13 can be individually brought into contact with a side of the sample liquid chip 40 (i.e., the cell wall 42a) that is opposite from the rotation table 11. This arrangement is suitable for efficiently realizing holding of the sample liquid chips 40 on the rotation table 11, which is kept at a constant temperature, movement of the heating block 12 for coming into contact with the sample liquid chips 40 (operation for temperature increase of the sample liquid 50) and movement of the cooling block 13 for coming into contact with the sample liquid chips 40 (operation for temperature reduction of the sample liquid 50).

As noted before, in the temperature controlling unit X1, the rotation table 11 has a holding surface 11a for holding the sample liquid chips 40 and is rotatable around the axis Ax perpendicular to the holding surface 11a. Further, each of the heating block 12 and the cooling block 13 faces the holding surface 11a of the rotation table 11 and is movable toward and away from the holding surface 11a. This arrangement is suitable for efficiently realizing holding of the sample liquid chips 40 on the rotation table 11, which is kept at a constant temperature, movement of the heating block 12 for coming into contact with the sample liquid chips 40 (operation for temperature increase of the sample liquid 50) and movement of the cooling block 13 for coming into contact with the sample liquid chips 40 (operation for temperature reduction of the sample liquid 50).

As described above, in the temperature controlling unit X1, the holding surface 11a includes the first region S_1 configured to hold a plurality of sample liquid chips 40 in contact with the sample liquid chips, and the second region S_2 configured to hold a plurality of sample liquid chips 40 in contact with the sample liquid chips. Moreover, each of the heating block 12 and the cooling block 13 is configured to come into contact with a plurality of sample liquid chips 40 held in the first region S_1 when the heating block or the cooling block faces the first region S_1 , and configured to come into contact with a plurality of sample liquid chips 40 held in the second region S_2 when the heating block or the cooling block faces the second region S_2 . With this arrangement, it is possible to perform in parallel the temperature increase step with respect to the sample liquid 50 in the sample liquid chips 40 in the first region S_1 by the heating block 12 and the temperature reduction step with respect to the sample liquid 50 in the sample liquid chips 40 in the second region S_2 by the cooling block 13. Further, it is possible to perform in parallel the temperature increase step with respect to the sample liquid 50 in the sample liquid chips 40 in the second region S_2 by the heating block 12 and the temperature reduction step with respect to the sample liquid 50 in the sample liquid chips 40 in the first region S_1 by the cooling block 13.

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As described above, in the temperature controlling unit X1, the first region S_1 and the second region S_2 are configured to hold a plurality of sample liquid chips 40 such that the sample liquid chips 40 are arranged on a circle (imaginary circle) around the axis Ax. This arrangement allows switching the position of the sample liquid chips 40 held in the first region S_1 and the position of the sample liquid chips 40 held in the second region S_2 by 180° rotation of the rotation table 11 or the holding surface 11a (rotation about the axis Ax).

As described above, in the temperature controlling unit X1, the sample liquid chip 40 includes cell walls 41a and 42a facing and spaced from each other, and a sample liquid cell 43 for receiving sample liquid 50 is defined between the cell walls 41a and 42a. Further, the rotation table 11 can hold the sample liquid chip 40 in contact with the cell wall 41a of the sample liquid chip 40, the heating block 12 can come into contact with the cell wall 42a of the sample liquid chip 40, and the cooling block 13 can also come into contact with the cell wall 42a of the sample liquid chip 40. This arrangement is suitable for efficient heat transfer between sample liquid 50 as a temperature control target and the heating block 12, and heat transfer between the sample liquid 50 and the cooling block 13.

As described above, in the temperature controlling unit X1, the maximum dimension of the sample liquid cell 43 in a direction perpendicular to the spacing direction (vertical direction in FIG. 5B) of the cell walls 41a and 42a is larger than the maximum dimension of the sample liquid cell 43 in the spacing direction. That is, the sample liquid cell 43 for receiving the sample liquid as a temperature control target is shallow. This arrangement is suitable for increasing the surface area of the sample liquid 50 per unit volume. A large surface area per unit volume of the sample liquid 50 contributes to efficient heat transfer between the sample liquid 50 and the heating block 12 and the heat transfer between the sample liquid 50 and the cooling block 13.

As described above, in the temperature controlling unit X1, the heating block 12 and the cooling block 13 include projections 12a and projections 13a, respectively, for coming into contact with the cell walls 42. This arrangement is suitable for allowing local heat transfer from the heating block 12 to the sample liquid 50 in the sample liquid cell 43 and local heat transfer from the sample liquid 50 in the sample liquid cell 43 to the cooling block 13. Realizing local heat transfer contributes to enhancement of heat transfer efficiency.

EXAMPLE

The above-described temperature controlling unit X1 was used, and temperature change of a liquid as a temperature control target was measured. Specifically, these were performed as follows.

First, a sample liquid chip 40 with a thermocouple inserted in the sample liquid cell 43 was prepared, and the sample liquid chip 40 was set in the first region S_1 of the holding surface 11a of the rotation table 11. Then, sample liquid 50 was introduced into the sample liquid cell 43 and mineral oil 60 was supplied into the liquid retaining space 44 in the same manner as shown in FIGS. 6A-6C. The thermocouple of the sample liquid chip 40 was arranged to constantly measure the temperature of the sample liquid 50 in the sample liquid cell 43 by utilizing a circuit provided at the rotation table 11. By operating the rotation table 11, the heating block 12 and the cooling block 13 of the temperature controlling unit X1, the thermal cycle consisting of the temperature increase step of Step 1, the temperature reduction step of Step 2 and the temperature maintaining step of Step 3-5 was repetitively

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performed with respect to the sample liquid **50** in the sample liquid cell **43** of the sample liquid chip **40**, in the same manner as described above with respect to the sample liquid **50** in the sample liquid cells **43** of the sample liquid chips **40** of the first group.

In this Example, the room temperature was 25° C., and the higher target temperature T_H and the lower target temperature T_L for the sample liquid **50** were set to 95° C. and 62° C., respectively. The temperature of the holding surface **11a** of the rotation table **11** (first temperature T_1) was set to 73° C., the temperature of the heating block **12** (second temperature T_2) was set to 120° C., and the temperature of the cooling block **13** (third temperature T_3) was set to 40° C. The temperature increase step was performed for six seconds, the temperature reduction step was performed for four seconds, and the temperature maintaining step was performed more than 16 seconds. In the temperature increase step of this Example, the heating block **12** was separated from the cell wall **42a** of the sample liquid chip **40** when the temperature of the sample liquid **50** reached the higher target temperature T_H . In the temperature reduction step of this Example, the cooling block **13** was separated from the cell wall **42a** of the sample liquid chip **40** one hundred milliseconds before the time when the temperature of the sample liquid **50** was expected to reach the lower target temperature T_L (the expected time determined in advance based on experiments or the like).

Part of the temperature change measured in this Example is shown in the graph of FIG. 15. In the graph of FIG. 15, the horizontal axis indicates time (second), whereas the vertical axis indicates sample liquid temperature (° C.). It is clear from the temperature change shown in the graph of FIG. 15 that the temperature controlling unit **X1** can change the temperature of the sample liquid **50** (liquid) quickly and precisely.

COMPARATIVE EXAMPLE

The temperature controlling unit **X1**, with the temperature control function of the rotation table **11** stopped, was used, and temperature change of a liquid as a temperature control target was measured. Specifically, these were performed as follows.

Similarly to the above-described Example, a sample liquid chip **40** with a thermocouple (and with the sample liquid cell **43** containing sample liquid **50**) was prepared and set in the first region S_1 of the holding surface **11a**. Similarly to the Example, the thermocouple of the sample liquid chip **40** was arranged to constantly measure the temperature of the sample liquid **50** in the sample liquid cell **43**. In this Comparative Example, the room temperature was 25° C., and the higher target temperature T_H and the lower target temperature T_L for the sample liquid **50** were set to 95° C. and 50° C., respectively. In this Comparative Example, the temperature of the heating block **12** (second temperature T_2) was set to 100° C., and the temperature of the cooling block **13** (third temperature T_3) was set to 50° C. By operating the rotation table **11** (the temperature control function stopped), the heating block **12** and the cooling block **13** of the temperature controlling unit **X1**, the thermal cycle consisting of a predetermined temperature increase step and a predetermined temperature reduction step was repetitively performed with respect to the sample liquid **50** in the sample liquid cell **43** of the sample liquid chip **40**. In the temperature increase step, the heating block **12** was separated from the cell wall **42a** of the sample liquid chip **40** when the temperature of the sample liquid **50** reached 95° C., which was the higher target temperature T_H . In the temperature reduction step, the cooling block **13** was

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separated from the cell wall **42a** of the sample liquid chip **40** when the temperature of the sample liquid **50** reached 50° C., which was the lower target temperature T_L .

The temperature change measured in this Comparative Example is shown in the graph of FIG. 16. In the graph of FIG. 16, the horizontal axis indicates time (second), whereas the vertical axis indicates sample liquid temperature (° C.). It is clear from the temperature change shown in the graph of FIG. 16 that it is difficult to change the temperature of the sample liquid **50** (liquid) quickly and precisely according to the Comparative Example. In the temperature increase step of the Comparative Example, it took about 80 seconds to raise the temperature of the sample liquid **50** from about 50° C. to about 95° C. In the temperature reduction step of this Comparative Example, it took about 95 seconds to reduce the temperature of the sample liquid from about 95° C. to about 50° C.

The invention claimed is:

1. A temperature controlling unit comprising:

a holder configured to hold a liquid receiver containing a liquid in contact with the liquid receiver and to maintain a first temperature for keeping the liquid at a lower target temperature;

a heating block configured to increase the temperature of the liquid through contact with the liquid receiver and to move relative to the liquid receiver, the heating block being further configured to maintain a second temperature higher than a higher target temperature that is higher than the lower target temperature, the heating block being spaced apart from the holder when contacting the liquid receiver; and

a cooling block configured to reduce the temperature of the liquid through contact with the liquid receiver and to move relative to the liquid receiver, the cooling block being further configured to maintain a third temperature lower than the lower target temperature, the cooling block being spaced apart from the holder when contacting with the liquid receiver,

wherein the heating block and the cooling block are configured to move relative to each other, so that the heating block and the cooling block are capable of moving relative to the liquid receiver independently of each other.

2. The temperature controlling unit according to claim 1, wherein the first temperature is selected from the group consisting of a temperature equal to the lower target temperature, a temperature higher than the lower target temperature and lower than the higher target temperature, and a temperature lower than the lower target temperature and higher than the third temperature.

3. The temperature controlling unit according to claim 1, wherein:

the heating block contacts a side of the liquid receiver that is opposite from the holder, and
the cooling block contacts a side of the liquid receiver that is opposite from the holder.

4. The temperature controlling unit according to claim 1, wherein:

the holder comprises a surface configured to hold the liquid receiver and is rotatable about an axis perpendicular to the surface; and
each of the heating block and the cooling block faces the surface and is movable toward and away from the surface.

5. The temperature controlling unit according to claim 4, wherein:

the holding surface comprises a first region configured to hold a liquid receiver containing a liquid in contact with

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the liquid receiver and a second region configured to hold a liquid receiver containing a liquid in contact with the liquid receiver; and

each of the heating block and the cooling block is configured to move closer to and contact the liquid receiver held in the first region when facing the first region and is configured to move closer to and contact the liquid receiver held in the second region when facing the second region.

6. The temperature controlling unit according to claim 4, wherein:

the holding surface comprises a first region configured to hold a plurality of liquid receivers each containing a liquid in contact with a liquid receiver and a second region configured to hold a plurality of liquid receivers each containing a liquid in contact with a liquid receiver; and

each of the heating block and the cooling block is configured to move closer to and contact the plurality of liquid receivers held in the first region when facing the first region and is configured to move closer to and contact the plurality of liquid receivers held in the second region when facing the second region.

7. The temperature controlling unit according to claim 6, wherein the first region and the second region are configured to hold the plurality of liquid receivers such that the liquid receivers are arranged in a circle around the axis.

8. The temperature controlling unit according to claim 1, wherein:

the liquid receiver comprises a first cell wall and a second cell wall facing and spaced from each other, and a cell configured to receive a liquid defined between the first cell wall and the second cell wall;

the holder is configured to hold the liquid receiver in contact with the first cell wall of the liquid receiver;

the heating block is configured to contact the second cell wall of the liquid receiver; and

the cooling block is configured to contact the second cell wall of the liquid receiver.

9. The temperature controlling unit according to claim 8, wherein a maximum dimension of the cell in a direction perpendicular to a spacing direction in which the first cell and

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the second cell are spaced from each other is larger than a maximum dimension of the cell in the spacing direction.

10. The temperature controlling unit according to claim 8, wherein each of the heating block and the cooling block comprises a projection configured to contact the second cell wall.

11. A method for controlling temperature of a liquid comprising:

increasing the temperature of a heating block kept at a temperature higher than a higher target temperature for a liquid into contact with a liquid receiver containing the liquid to increase the temperature of the liquid; and

decreasing the temperature of a cooling block kept at a cooling temperature lower than a lower target temperature that is lower than the higher target temperature into contact with the liquid receiver to reduce the temperature of the liquid;

wherein the temperature reducing step is performed with a lower target temperature maintaining member in contact with and holding the liquid receiver, the cooling block being spaced apart from the lower target temperature maintaining member for the temperature reducing step, the lower target temperature maintaining member being kept at a temperature selected from the group consisting of a temperature equal to the lower target temperature, a temperature higher than the lower target temperature and lower than the higher target temperature, and a temperature lower than the lower target temperature and higher than the cooling temperature,

wherein the heating block and the cooling block are configured to move relative to each other, so that the heating block and the cooling block are capable of moving relative to the liquid receiver independently of each other.

12. The method according to claim 11, wherein, in the temperature increasing step, the heating block is separated from the liquid receiver when the temperature of the liquid has reached the higher target temperature.

13. The method according to claim 11, wherein, in the temperature reducing step, the cooling block is separated from the liquid receiver before the temperature of the liquid reaches the lower target temperature.

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